TRAFFIC IMPACT AND ACCESS STUDY

PROPOSED RESIDENTIAL DEVELOPMENT

Salisbury Pine Tree Estates Holden, Massachusetts

Prepared for: Holden Realty Trust Holden, MA

October 2019

MDM TRANSPORTATION CONSULTANTS, INC. Planners & Engineers

Traffic Impact and Access Study

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MDM Transportation Consultants, Inc. (MDM) has prepared this initial Transportation Impact and Access Study (TIAS) for proposed residential development to be located off of Pine Tree Road and Bailey Road in Holden, Massachusetts. The location of the site relative to adjacent roadways is shown in Figure 1. This report documents existing operational and safety-related characteristics of roadways serving the development site, estimates future year operating characteristics of these roadways independent of the development, estimates development-related trip generation, and identifies incremental impacts of site-related traffic. Improvements are recommended that will offset project-related traffic increases and enhance the safety of traffic flow.

This TIAS has been developed in conformance with guidelines for preparation of traffic studies as jointly issued by the Commonwealth of Massachusetts Executive Office of Energy & Environmental Affairs/Massachusetts Department of Transportation (EEA/MassDOT).

E.1 PROJECT DESCRIPTION

The project site includes approximate 21 acres of land located between Pine Tree Road and Bailey Road in Holden, Massachusetts. The existing site is comprised of undeveloped land, a single-family home (#124 Bailey Road), and an abandoned single-family home off of Salisbury Street.

Under the proposed development plan, a 102 unit (12 single family and 90 multifamily) residential development will be constructed with off-street parking for approximately 204 vehicles. The existing single-family home located at 124 Bailey Road will remain with access via a new driveway connection to the proposed subdivision roadway. Access to the site will be provided by a full-access unsignalized driveway along Salisbury Street via the existing Pine Tree Road and a full-access unsignalized driveway along Bailey Road just south of house #124. Salisbury Street and Bailey Road are both public ways and are owned and controlled by the Town of Holden.

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Pine Tree Road is an existing "way in existence" stub roadway currently providing access to two multi-family residential buildings (totaling 8 apartment units). Under the proposed development program, the 8 apartment units will continue to have access from Pine Tree Road. One of the proposed single-family residential units will have direct access to Salisbury Street.

E.2 STUDY AREA

This TIAS evaluates transportation characteristics of roadways and intersections that provide a primary means of access to the site, and that are likely to sustain a measurable level of traffic impact from the proposed development. The study area includes the following intersections:

- □ Salisbury Street at Subdivision Site Drive (Unsignalized)
- □ Salisbury Street at Main Street (Route 122A) (Signalized)
- □ Bailey Road at Subdivision Site Drive (Unsignalized)
- □ Bailey Road at Main Street (Route 122A) (Unsignalized)

E.3 SUMMARY OF ANALYSIS AND FINDINGS

Capacity analyses were conducted for each study area intersection to quantify existing and future year traffic operations with and without the development for the weekday morning and weekday evening peak hours. These hours coincide with peak traffic activity of the proposed residential development and the adjacent streets.

The analyses presented in this TIAS are based on industry-standard trip rates published by the Institute of Transportation Engineers (ITE). The proposed development is estimated to generate approximately 52 vehicle trips during the weekday morning peak hour (12 entering and 40 exiting) and 66 vehicle trips during the weekday evening peak hour (42 entering and 24 exiting). On a daily basis, the development is estimated to generate approximately 754 vehicle trips on a weekday.

Under Build conditions, capacity analyses indicate that the Site Driveway approaches to Salisbury Street and Baily Road will operate under capacity at LOS B or better during the weekday morning and weekday evening peak hours. Mainline (through) travel along Main Street will continue to operate unimpeded with minimal delay. The minor street approaches at the intersection of Main Street (Route 122A) and Bailey Road/ Mayo Drive currently operate with long delays during the peak hours. Likewise, left turns from Main Street (again low volumes) experience delays, resulting in use of the paved shoulders to by-pass left turning vehicles. Operations at the signalized Main Street at Salisbury Street intersection are projected to be LOS C or better during peak hours

The proposed development is expected to have a minimal impact on the study area intersections as there will be a nominal overall change in level of service and operations of the study intersections under future conditions with the development. Adequate capacity is available under future Build conditions on both Salisbury Street and Bailey Road to accommodate the site use.

<u>E.4 RECOMMENDATIONS AND CONCLUSIONS</u>

Traffic impacts associated with the residential development are not expected to notably affect travel or safety conditions in the site vicinity. However, MDM recommends access-related improvements aimed at enhancing traffic operations and/or travel safety. Specific recommendations are as follows:

Pine Tree Road at Salisbury Street. The existing Pine Tree Road and Salisbury Street intersection will serve as primary access to the site. Currently, no traffic control or marked pedestrian crossing is present on the Pine Tree Road eastbound approach. MDM recommends the following improvements:

- □ A STOP sign (R1-1) and STOP line pavement markings is recommended on the Pine Tree Road approach to Salisbury Street. A marked crosswalk and ADA compliant ramps should be installed at the intersection across Pine Tree Road.
- □ A sidewalk is recommended on Pine Tree Road to connect the site with the existing sidewalk system on the western side of Salisbury Street which extends from Main Street to the Dawson Elementary School.
- Plantings (shrubs, bushes) and structures (walls, fences, etc.) should be maintained at a height of 2 feet or less within the Salisbury Street layout in vicinity of the site driveway to provide unobstructed sight lines.

Bailey Road at Proposed Site Drive. The proposed site driveway will connect the site with Bailey Road just south of the existing garage for #124 Bailey Road. MDM recommends that the Applicant implement the following items:

- □ A STOP sign (R1-1) and STOP line pavement markings should be installed on the Site Drive approach to Bailey Road.
- □ Plantings (shrubs, bushes) and structures (walls, fences, etc.) should be maintained at a height of 2 feet or less within the Bailey Road layout in vicinity of the site driveway to provide unobstructed sight lines.

In summary, adequate capacity is available under future Build conditions on both Salisbury Street and Bailey Road to accommodate the site use. The project is not projected to significantly change any reported operating levels compared to future No-Build conditions. Proposed access improvements will provide ample capacity to accommodate site-generated traffic while also enhancing safety and capacity.

This report presents a transportation impact and access evaluation for a proposed 112-unit residential development to be located off of Pine Tree Road and Bailey Road in Holden, Massachusetts. The location of the site relative to adjacent roadways is shown in Figure 1. The evaluation includes existing traffic operations in the study area and assesses incremental impacts on area roadways under future year conditions with and without the development.

This TIAS has been developed in conformance with guidelines for preparation of traffic studies as jointly issued by the Commonwealth of Massachusetts Executive Office of Energy & Environmental Affairs/Massachusetts Department of Transportation (EEA/MassDOT).

1.1 PROPOSED DEVELOPMENT

The project site includes approximate 21 acres of land located between Pine Tree Road and Bailey Road in Holden, Massachusetts. The existing site is comprised of undeveloped land, a single-family home (#124 Bailey Road), and an abandoned single-family home off of Salisbury Street.

Under the proposed development plan, a 102 unit (12 single family and 90 multifamily) residential development will be constructed with off-street parking for approximately 204 vehicles. The existing single-family home located at 124 Bailey Road will remain with access via a new driveway connection to the proposed subdivision roadway. Access to the site will be provided by a full-access unsignalized driveway along Salisbury Street via the existing Pine Tree Road and a full-access unsignalized driveway along Bailey Road just south of house #124. Salisbury Street and Bailey Road are both public ways and are owned and controlled by the Town of Holden.



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Figure 1

Site Location

Pine Tree Road is an existing "way in existence" stub roadway currently providing access to two multi-family residential buildings (totaling 8 apartment units). Under the proposed development program, the 8 apartment units will continue to have access from Pine Tree Road. One of the proposed single-family residential units will have direct access to Salisbury Street. The preliminary Site layout prepared by Places Associates; Inc. is presented in Figure 2.

1.2 STUDY METHODOLOGY

This transportation impact and access evaluation was conducted in accordance with EEA/MassDOT guidelines and consists of several steps. The first step documents existing conditions in the transportation study area including an inventory of roadway geometry, observed traffic volumes, and safety characteristics. Next, future year traffic conditions are forecast that account for other planned area developments, normal area growth, and development-related traffic increases. The third step quantifies operating characteristics of the primary study intersections. Specific attention is given to the incremental impacts of the proposed development. Finally, off-site improvements are identified to address specific development-related access needs as required.

1.3 STUDY AREA

This TIAS evaluates transportation characteristics of roadways and intersections that provide a primary means of access to the site, and that are likely to sustain a measurable level of traffic impact from the development. The study area includes the following intersections, which are also identified in Figure 1:

- □ Salisbury Street at Subdivision Site Drive (Unsignalized)
- □ Salisbury Street at Main Street (Route 122A) (Signalized)
- □ Bailey Road at Subdivision Site Drive (Unsignalized)
- □ Bailey Road at Main Street (Route 122A) (Unsignalized)

Source: Places Associates, Inc. salsbury street Table Office Table Office Table Office A. D S. The state of the s 日 H. Pine Tree Road Farmers Way The Part of the Pa Henry Way ولا الما المولد النا الم STATE AND 国 1 [B] 101 0 k T. SI-ENWART AN Traffic Impact & Access Study Holden, Massachusetts Bailey Road of soldings of the soldings of Scale: Not to Seale North

Preliminary Site Layout

Figure 2

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In order to provide a basis for quantifying the transportation impacts of the development, the existing roadway system and the existing traffic operations of study area roadways were reviewed. This section describes the existing traffic characteristics and operations of roadways and intersections within the study area. Specifically, this section presents an overview of the traffic data collection program, existing traffic volumes, safety data, and public transportation facilities serving the area.

2.1 STUDY AREA ROADWAY NETWORK

The study area roadways and intersections are described briefly in this section. A general description of the physical roadway and intersection features is provided. The study area and intersections are depicted in Figure 1.

2.1.1 Roadways

Main Street (Route 122A)

Main Street (Route 122A) is an east-west roadway, in the immediate study area, under State (MassDOT) jurisdiction and classified as an Urban Other Principal Arterial Roadway. Main Street (Route 122A) provides a connection between Grove Street (Route 122A) to the southeast in the City of Worcester and North Main Street to the southwest in the Town of Holden. In the study area, the roadway width is approximately 44 feet wide and generally provides one lane of travel in each direction separated by a double yellow centerline and 10-foot paved shoulders. Near major intersections including Salisbury Street, Main Street (Route 122A) provides two lanes of travel in each direction separated by a double yellow centerline and 2-foot paved shoulders. The posted regulatory speed limit along Main Street (Route 122A) in the immediate study area is 35 miles per hour (mph). Land use along Main Street (Route 122A) in the immediate project area includes a mix of commercial, residential, and industrial land uses.

Salisbury Street

Salisbury Street is a north-south roadway under Local (Town) jurisdiction and is classified by MassDOT as an Urban Minor Arterial roadway. Salisbury Street connects Main Street (Route 122A) to the north with Salisbury Street in the City of Worcester to the south. In the project area Salisbury Street has a width of approximately 28 feet wide and provides one lane of travel in each direction with 2-foot paved shoulders. The posted regulatory speed limit along Salisbury Street in the immediate study area is 35 miles per hour (mph). Land use along Salisbury Street is primarily residential but also includes the Dawson Elementary School which is located approximately ¼ mile to the south.

Bailey Road

Bailey Road is a north-south roadway under Local (Town) jurisdiction and is classified by MassDOT as an Urban Local roadway. Bailey Road connects Main Street (Route 122A) to the north with Reservoir Street in the Town of Holden. In the project area Bailey Road has a width of approximately 21 feet and provides one lane of travel in each direction. The posted advisory speed limit along Bailey Road in the immediate study area is 25 miles per hour (mph). Land use along Bailey Road is includes residential land uses and undeveloped land.

Pine Tree Road

Pine Tree Road is an east-west roadway under Local (City) jurisdiction and is classified by MassDOT as an Urban Local roadway. Pine Tree Road is a "way in existence" stub road that connects several land parcels with Salisbury Street. Pine Tree Road has a width of approximately 30 feet and provides one lane of travel in each direction. There is no regulatory posted speed limit on Pine Tree Road. Land use along Pine Tree Road includes two residential apartment buildings with a total of eight (8) units and provides access to the proposed development site.

2.1.2 Intersections

Main Street (Route 122A) at Salisbury Street

Salisbury Street meets Main Street (Route 122A) to form a three-way, signalized intersection. The Main Street (Route 122A) eastbound approach to the intersection provides a through travel lane and a shared through/right travel lane. The Main Street (Route 122A) westbound approach to the intersection provides a shared left/through travel lane and a through travel lane. The Salisbury Street approach provides an exclusive left turn lane and an exclusive right turn lane on a downgrade of approximately 6%. Land use at the intersection consists of Sunnyside Motor Company, Quick Lane, and a residential home.

Main Street (Route 122A) at Bailey Road/ Mayo Drive

Bailey Road and Mayo Drive meet Main Street (Route 122A) to form a four-way, unsignalized intersection. The Main Street eastbound and westbound approaches to the intersection provide single travel lanes and operate freely. The Bailey Road northbound approach provides a single travel lane and is under STOP control. The Mayo Drive southbound approach provides a single travel lane and is under STOP Control. Land use at the intersection includes several office buildings, Lawton's Optical World, and an undeveloped lot.

2.2 EXISTING TRAFFIC VOLUMES

Traffic-volume data used in this study were obtained by manual and mechanical methods. Manual turning movement counts (TMCs) were conducted along study area roadways and intersections in May 2019. Traffic data were collected during the weekday morning (7:00 AM to 9:00 AM) and weekday evening (4:00 PM to 6:00 PM) peak periods to coincide with peak traffic activity of the proposed residential development and the adjacent streets. Automated traffic recorder counts (ATR's) were also conducted in May 2019. Traffic count data is provided in the Appendix.

2.2.1 Daily Traffic

Daily traffic volumes along Salisbury Street and Bailey Road in the site vicinity were obtained by mechanical methods using ATR's in May 2019. The results of the counts are summarized in **Table 1** and are discussed below.

TABLE 1 EXISTING TRAFFIC-VOLUME SUMMARY

Time Period	Daily Volume (vpd) ¹	Percent Daily Traffic²	Peak Hour Volume (vph) ³	Peak Flow Direction ⁴	Peak Hour Directional Volume (vph)
Salisbury Street north of Pine Ti	ree Road				(T)
Weekday Morning Peak Hour	6,740	7%	495	62% SB	305
Weekday Evening Peak Hour	6,740	9%	579	55% NB	316
Bailey Road south of Thorny Le	a Road				
Weekday Morning Peak Hour	1,080	10%	103	66% SB	68
Weekday Evening Peak Hour	1,080	11%	115	63% SB	72

^{&#}x27;Two-way daily traffic expressed in vehicles per day without seasonal adjustment.

²The percent of daily traffic that occurs during the peak hour.

³Two-way peak-hour volume expressed in vehicles per hour.

⁴NB = Northbound, SB = Southbound

As summarized in Table 1:

- Salisbury Street north of Pine Tree Road: Daily traffic volume on Salisbury Street north of Pine Tree Road is approximately 6,740 vehicles per day (vpd) on weekdays. Weekday peak hour traffic flow on Salisbury Street is approximately 7 to 9 percent of daily flow with directional flow split heavier southbound during the weekday morning peak hour and heavier northbound during the weekday evening peak hour, consistent with commuter-related travel.
- Bailey Road south of Thorny Lea Road: Daily traffic volume on Bailey Road south of Thorny Lea Road is approximately 1,080 vehicles per day (vpd) on weekdays. Weekday peak hour traffic flow on bailey Road is approximately 10 to 11 percent of daily flow with directional flow split heavier southbound during the weekday morning peak hour and weekday evening peak hour.

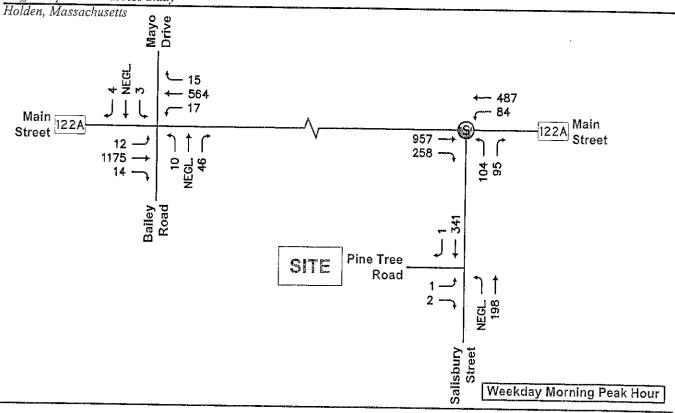
2.2.2 Peak-Hour Traffic

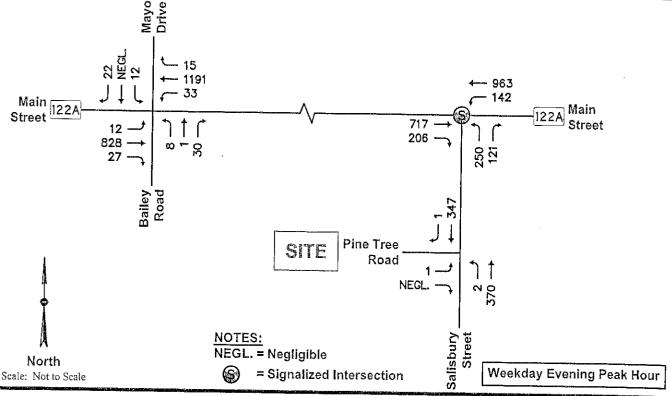
Manual turning movement counts (TMCs) were conducted along study area roadways and intersections in May 2019. This traffic data was collected during the weekday morning (7:00 AM to 9:00 AM) and weekday evening (4:00 PM to 6:00 PM) peak periods to coincide with peak traffic activity of the proposed residential development and the adjacent streets.

Review of MassDOT permanent count station data indicates that May is a slightly above-average traffic month. Therefore, no adjustment (reduction) in the observed traffic volumes was made as a conservative measure. Permanent count station data is provided in the **Appendix**. The resulting existing weekday morning and weekday evening peak-hour traffic volumes for study intersections are depicted in **Figure 3**.

2.2.3 Measured Travel Speeds

Vehicle speeds were obtained for Salisbury Street northbound and southbound travel directions and Bailey Road northbound and southbound travel directions. The study was performed in May 2019. Table 2 summarizes the posted speed and observed average and 85th percentile travel speeds for the two locations and field data is provided in the Appendix.





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Figure 3

2019 Baseline Conditions Weekday Peak Hour Volumes

TABLE 2 SPOT SPEED STUDY RESULTS

	Travel Speeds						
Approach/ Travel Direction	Posted	Mean ¹	85th Percentile ²				
Salisbury Street near Pine Tree Road							
Northbound	35	29	34				
Southbound	35	27	31				
Bailey Road near Thorny Lea Road							
Northbound	25	30	36				
Southbound	25	30	36				

Arithmetic mean

As summarized in Table 2, the mean (average) travel speed on Salisbury Street traveling northbound is 29 mph and the 85th percentile travel speed is 34 mph. In the southbound direction, the mean travel speed is 27 mph and the 85th percentile travel speed is 31 mph. The mean (average) travel speed on Bailey Road traveling northbound and southbound is 30 mph and the 85th percentile travel speed is 36 mph.

2.3 SAFETY

In order to identify crash trends and safety characteristics for study area intersections, crash data were obtained from MassDOT for the Town of Holden for the five-year period covering 2014 through 2018 (the most recent data currently available from MassDOT). A summary of the crash data with crash rates for the study intersection with reported crashes is detailed in Table 3 with detailed data provided in the Appendix.

Crash rates were calculated for the study intersection as reported in Table 3. This rate quantifies the number of crashes per million entering vehicles. MassDOT has determined the official District 3 (which includes the Town of Holden) crash rate to be 0.61 for unsignalized intersections and 0.89 for signalized intersections. This rate represents MassDOT's "average" crash experience for District 3 communities and serves as a basis for comparing reported crash rates for the study intersections. Where calculated crash rates notably exceed the district average, some form of safety countermeasures may be warranted. A review of Highway Safety Improvement Project (HSIP) locations was also conducted.

² The speed at or below which 85 percent of the vehicles are traveling

TABLE 3 INTERSECTION CRASH SUMMARY — 2014 THROUGH 2018 $^{\scriptscriptstyle 1}$

Data Category	Main St (Route 122A) at Bailey Rd & Mayo Dr	Main St (Route 122A) at Salisbury Street	Salisbury St at Pine Tree Rd		
Traffic Control	Unsignalized	Signalized	Unsignalized		
Crash Rate ²³	0.23	0,37	0.00		
MHD District 3 Avg. ³	0.61	0.89	0.61		
Year:					
2014	2	2	0		
2015	1	8	Ö		
2016	4	5	0		
2017	1	3	0		
<u>2018</u>	<u>2</u>	<u>3</u>	<u>0</u>		
Total	12	21	0		
Туре:			Ü		
Angle	4	3	0		
Rear-End	3	12	0		
Head-On	0	0	0		
Sideswipe	4	5	0		
Single Vehicle	1	1	0		
Other/Unknown	0	0	-		
Severity:					
P. Damage Only	9	17	0		
Personal Injury	3	4	0		
Fatality	0	0	0		
Other/Unknown	0	0	0		
Conditions:					
Dry	7	16	0		
Wet	1	3	0		
Snow	4	2	0		
Other	0	0	0		
Гіте:					
7:00 to 9:00 AM	3	1	0		
4:00 to 6:00 PM	0	2	0		
Rest of Day ource: MassDOT Crash Datab	9	18	0		

² Crashes per million entering vehicles

³ District 3 average = 0.61 for unsignalized intersections and 0.89 for signalized intersections

As summarized in Table 3:

- A total of twelve (12) crashes were reported for the unsignalized intersection of Main Street (Route 122A) and Bailey Road/Mayo. The resulting crash rate of 0.23 is lower than the District 3 average. The reported crashes included eight (8) angle/ sideswipe type collisions, three (3) rear-end type collisions and one (1) single vehicle collision. Seventy-five percent (75%) of the crashes resulted in property-damage only, generally indicative of low-speed crashes. No fatalities or pedestrian-related incidents were reported during the study period.
- A total of twenty-one (21) crashes were reported for the signalized intersection of Main Street (Route 122A) and Salisbury Street. The resulting crash rate of 0.37 is lower than the District 3 average. The reported crashes included eight (8) angle/sideswipe type collisions, twelve (12) rear-end type collisions and one (1) single vehicle collision. Seventy-six percent (76%) of the crashes resulted in property-damage only, generally indicative of low-speed crashes. No fatalities or pedestrian-related incidents were reported during the study period.

In summary, the crash rates at the study intersections are all lower than the District 3 average crash rates and are not listed as an HSIP location. No immediate safety countermeasures are warranted based on the crash history at the study locations.

2.4 SIGHT LINE ANALYSIS

An evaluation of sight lines was conducted at the proposed site driveway locations to determine whether minimum recommended sight lines are available to safely exit onto Salisbury Street and Bailey Road. The evaluation documents existing sight lines for vehicles as they relate to Salisbury Street and Bailey Road with comparison to recommended guidelines.

The American Association of State Highway and Transportation Officials' (AASHTO) standards¹ reference two types of sight distance which are relevant at the proposed site driveway intersections at Salisbury Street and Bailey Road: stopping sight distance (SSD) and intersection sight distance (ISD). Sight lines for critical vehicle movements at the proposed site driveway intersections with Salisbury Street and Bailey Road were compared to recommended minimum SSD and ISD guidelines for the posted speed and observed average and 85th percentile travel speeds.

¹ A policy on Geometric Design of Highways and Streets, American Association of State Highway and Transportation Officials (AASHTO), 2004.

Stopping Sight Distance

Sight distance is the length of roadway visible to the motorist to a fixed object. The minimum sight distance available on a roadway should be sufficiently long enough to enable a below-average operator, traveling at or near a regulatory speed limit, to stop safely before reaching a stationary object in its path, in this case, a vehicle exiting onto Salisbury Street or Bailey Road. The SSD criteria are defined by AASHTO based on design and operating speeds, anticipated driver behavior and vehicle performance, as well as physical roadway conditions. SSD includes the length of roadway traveled during the perception and reaction time of a driver to an object, and the distance traveled during brake application on wet level pavement. Adjustment factors are applied to account for roadway grades when applicable.

SSD was estimated in the field using AASHTO standards for driver's eye (3.5 feet) and object height equivalent to the taillight height of a passenger car (2.0 feet) for the northbound and southbound Salisbury Street approaches to Pine Tree Road and for the northbound and southbound Bailey Road approaches to the proposed sub-division roadway (just south of 124 Bailey Road). Table 4 presents a summary of the available SSD as they relate to the proposed site driveways and AASHTO's recommended SSD. SSD calculations are provided in the Appendix.

TABLE 4
STOPPING SIGHT DISTANCE SUMMARY

		AASHTO	Recommended ¹
Approach/ Travel Direction	Available SSD	Regulatory Speed²	85 th Percentile Observed Travel Speed ³
alisbury Street Approach i	to Pine Tree Road		- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1
Northbound Southbound	>800 Feet 355 ± Feet	250 Feet 250 Feet	240 Feet 210 Feet
ailey Road Approach to P	roposed Site Driveway		
Northbound Southbound	525 ± Feet 360 ± Feet	155 Feet 155 Feet	260 Feet 260 Feet

¹Recommended sight distance based on AASHTO, A Policy on Geometric Design of Highways and Streets. Based on driver height of eye of 3.5 feet to object height of 2.0 feet.

 $^{^2}$ SRegulatiory Speed on Salisbury Street = 35 mph. Regulatory Speed on Bailey Road = 25 mph.

³85th Percentile travel speed on Salisbury Street: 34 mph NB and 31 mph SB. 85th Percentile travel speed on Bailey Road: 36 mph and SB.

As summarized in **Table 4**, analysis results indicate that, with the removal of existing the existing vegetation, trees, and physical features within the sight lines during the construction of the proposed sub-division roadways, the available sight lines to the site driveways will exceed AASHTO's recommended SSD criteria for both travel directions along Salisbury Street and Bailey Road.

Intersection Sight Distance

Clear sight lines provide sufficient sight distance for a stopped driver on a minor-road approach to depart from the intersection and enter or cross the major road. As stated under AASHTO's Intersection Sight Distance (ISD) considerations, "...If the available sight distance for an entering ...vehicle is at least equal to the appropriate stopping sight distance for the major road, then drivers have sufficient sight distance to avoid collisions...To enhance traffic operations, intersection sight distances that exceed stopping sight distances are desirable along the major road." AASHTO's ISD criteria are defined into several "cases". In this case, the proposed site driveway approaches to the intersections are proposed to be under STOP signal control and the ISD in question relates to the ability to turn left or turn right onto Salisbury Street or Bailey Road.

Available ISD was estimated in the field using AASHTO standards for driver's eye (3.5 feet), object height (3.5 feet) and decision point (8 to 14.5 feet from marked edge lines) for the northbound and southbound directions along Salisbury Street and Bailey Road. Table 5 presents a summary of the available ISD for the departure from Pine Tree Road to Salisbury Street and the Proposed Site Driveway to Bailey Road and AASHTO's recommended ISD.

TABLE 5
INTERSECTION SIGHT DISTANCE SUMMARY

		AASHT(O Minimum¹
View Direction	Available ISD	Regulatory Speed ²	85 th Percentile Speed ³
Pine Tree Road Departures to Sa	lisbury Street		
Looking North	325 ± Feet ⁴	250 Feet	210 Feet
Looking South	>800 Feet	250 Feet	240 Feet
Proposed Site Driveway Departi	ires to Bailey Road		
Looking North	340 ± Feet⁵	155 Feet	260 Feet
Looking South	510 ± Feet⁵	155 Feet	260 Feet

¹Recommended sight distance based on AASHTO, A Policy on Geometric Design of Highways and Streets. Based on driver height of eye of 3.5 feet and an object height of 3.5 feet and adjustments for roadway grade if required. Minimum value as noted represents SSD per AASHTO guidance.

²Regulatiory Speed on Salisbury Street = 35 mph. Regulatory Speed on Bailey Road = 25 mph.

³⁸⁵th Percentile travel speed on Salisbury Street: 34 mph NB and 31 mph SB. 85th Percentile travel speed on Bailey Road: 36 mph and SB.

⁴Assumes a position approximately 10 feet from the marked edge line to clearly see past an existing section of guardrail.

⁵ Assumes clearing of vegetation within the right-of-way and the re-location of a wooden fence at 124 Bailey Road.

The results of the ISD analysis presented in Table 5 indicate that, with the removal of existing the existing vegetation, trees, and physical features within the sight lines during the construction of the proposed sub-division roadways, the available intersection sight distance from the site driveways will satisfy AASHTO's recommended minimum criteria looking to the north and to the south onto Salisbury Street and Bailey Road.

In summary, analysis indicates that the criteria for SSD (a safety-based requirement) are satisfied for travel on Salisbury Street and Bailey Road as well as sight lines exiting Pine Tree Road onto Salisbury Street and the Proposed Site Driveway onto Bailey Road.

2.5 PUBLIC TRANSPORTATION

The Worcester Regional Transit Authority (WRTA) no longer operates fixed bus route service within the study area.

Evaluation of the proposed development impacts requires the establishment of a future baseline analysis condition. This section estimates future roadway and traffic conditions with and without the proposed development. To be consistent with EEA/EOT, a five-year planning horizon was selected.

To determine the incremental impact of new site-generated traffic volumes on the roadway network under future conditions, baseline traffic volumes in the study area were projected to a future year condition. Traffic volumes on the roadway network at that time, in the absence of the development (that is, the No-Build condition), would include existing traffic, new traffic due to general background traffic growth, and traffic related to specific developments by others that are currently under review at the local and/or state level. Consideration of these factors resulted in the development of No-Build traffic volumes. Anticipated site-generated traffic volumes were then superimposed upon these No-Build traffic-flow networks to develop future Build conditions.

The following sections provide an overview of planned roadway improvements in the study area, the future No-Build traffic volumes and projected Build traffic volumes.

3.1 BACKGROUND TRAFFIC GROWTH

Background traffic includes demand generated by other planned developments in the area as well as demand increases caused by external factors. External factors are general increases in traffic not attributable to a specific development and are determined using historical data.

3.1.1 Historical Area Growth

Nearby permanent count station data published by MassDOT indicates a 0.26 percent per year growth rate. For purposes of this evaluation, a 0.5-percent compounded annual growth rate is proposed (2.5 percent increase over a 5-year horizon). This growth rate is higher than historic rates and is also expected to account for any small fluctuation in hourly traffic as may occur from time to time in the study area and traffic associated with other potential small developments or vacancies in the area. MassDOT permanent count station data and background growth calculations are provided in the **Attachments**.

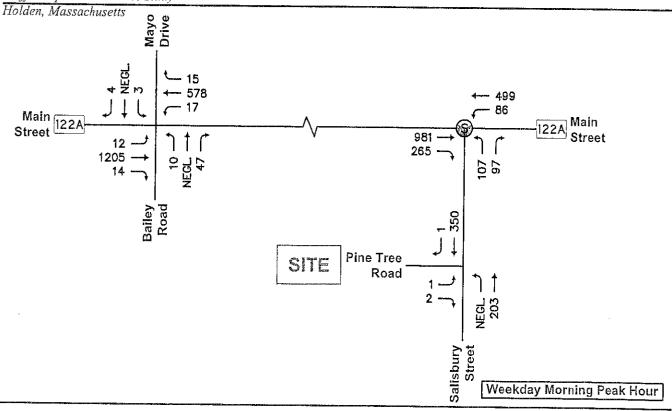
3.1.2 Background Development-Related Growth

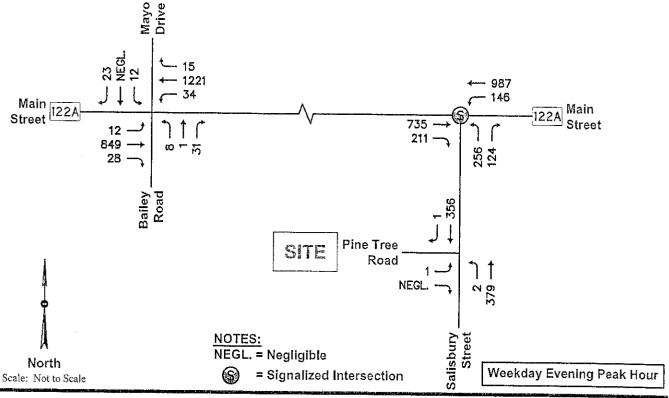
Development of future No-Build traffic volumes also considers traffic generated from specific area developments. Based on consultation with the Town of Holden Department of Growth Management and review of Massachusetts Environmental Policy Act (MEPA) files, there are several planned and or approved development projects in the vicinity of the project area that were not completed at the time the counts were conducted. Traffic associated with these developments was incorporated into the future year 2024 No-Build traffic networks. The following developments are expected to generate traffic which may to impact the study area intersections:

- □ 757 Salisbury Street: This development includes the construction of 123 age-restricted on Salisbury Street in Worcester, Massachusetts. Traffic associated with this development are negligible and can be accounted for in the 0.5-percent compounded annual growth rate over 5 years.
- Salisbury Hill: This development includes the construction of 114 additional age restricted units to Salisbury Hill condominium complex in Worcester, Massachusetts. Traffic associated with this development are negligible and can be accounted for in the 0.5-percent compounded annual growth rate over 5 years.

3.2 NO-BUILD TRAFFIC VOLUMES

Future No-Build traffic volumes are developed by increasing the existing (2019) volumes by approximately 2.5 percent (0.5 percent compounded annually over 5 years) to account for normal area growth. The resulting 2024 No-Build traffic volumes are displayed in Figure 4.





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Figure 4

2024 No-Build Conditions Weekday Peak Hour Volumes

3.3 SITE-GENERATED TRAFFIC

The trip generation estimates for the proposed residential are provided for the weekday morning and evening periods, which correspond to the critical weekday analysis periods for the proposed use and adjacent street traffic flow. New traffic generated by the project was estimated using trip rates published in ITE's *Trip Generation*² for Land Use Codes (LUCs) based on national trip rates for single-family detached housing (ITE LUC 210) and for multifamily housing (low-rise) (ITE LUC 220). Table 6 presents the trip-generation estimate for the proposed development based on ITE.

TABLE 6
TRIP-GENERATION SUMMARY

Peak Hour/Direction	Single Family (12 Units)	Multifamily (90 Units) ²	Total
Weekday Morning Peak Hour:			
Entering	2	10	12
<u>Exiting</u>	<u>7</u>	<u>33</u>	<u>40</u>
Total	9	43	52
Weekday Evening Peak Hour:			
Entering	8	34	42
Exiting	<u>4</u>	<u>20</u>	<u>24</u>
Total	12	54	66
Weekday Daily (24 hours):	114	640	754

Source: ITE Trip Generation, Tenth Edition; 2018.

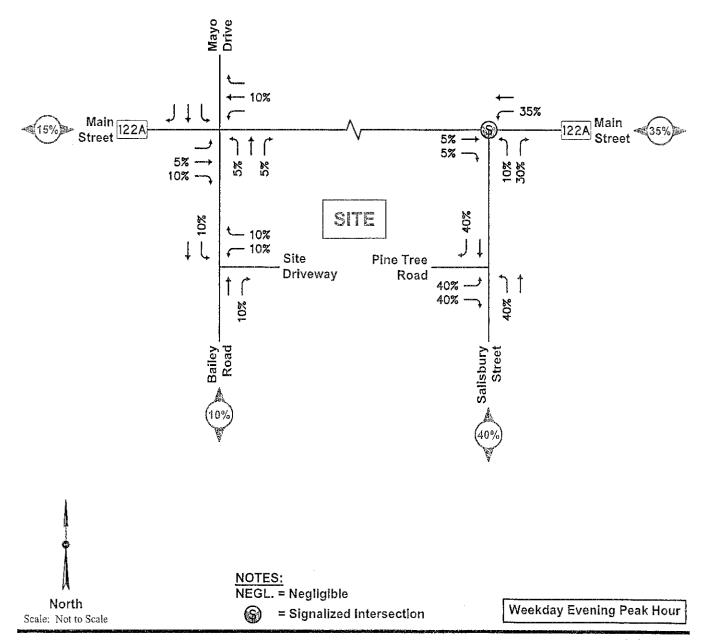
¹Based on ITE LUC 210 (Single Family Detached) applied to 10 Units and ITE LUC 220 (Multifamily Houseing (Low-Rise) applied to 102 units).

As summarized in **Table** 6, the proposed development is estimated to generate approximately 52 vehicle trips (12 entering and 40 exiting) during the weekday morning peak hour and 66 vehicle trips (42 entering and 24 exiting) during the weekday evening peak hour. On a daily basis, the proposed development is estimated to generate approximately 754 vehicle trips on a weekday.

3.4 TRIP DISTRIBUTION AND ASSIGNMENT

The distribution for projected traffic for the proposed residential is based primarily on Census 2010 statistics for employment for residents of Holden. Existing travel patterns, volumes of the adjacent roadway system, and locations of local employment centers were also considered. The resulting trip distribution is presented in Figure 5. Trip distribution calculations and Census 2010 data are provided in the Appendix.

² Trip Generation, Tenth Edition; Institute of Transportation Engineers; Washington, DC; 2018.



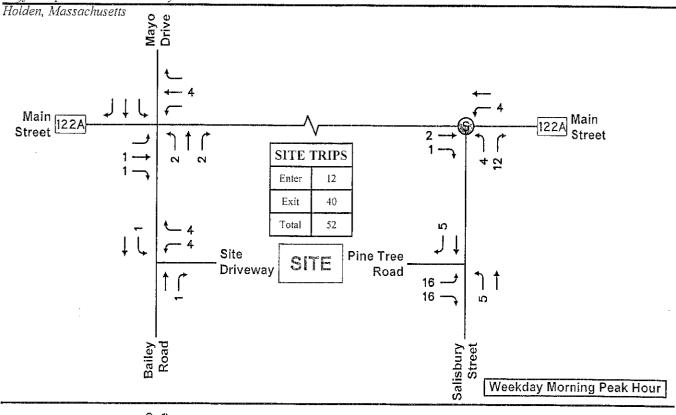
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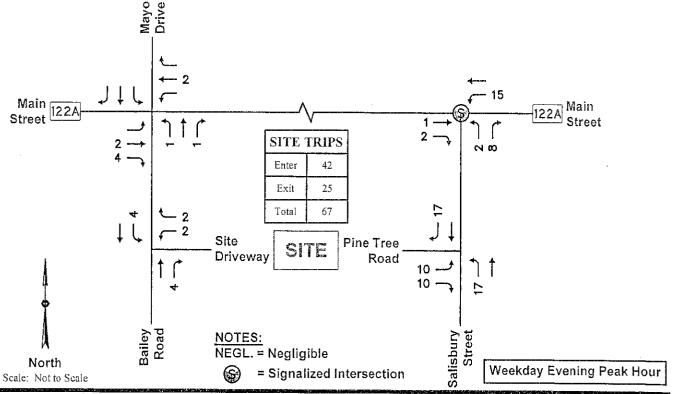
Figure 5

Trip Distribution Peak Hour Traffic Volumes Development-related trips for the residential development were assigned to the roadway network using the ITE trip-generation estimates shown in **Table 6** and the distribution patterns presented in **Figure 5**. New development-related trips at each intersection approach for the weekday morning and weekday evening peak hours are quantified in **Figure 6**.

3.5 BUILD TRAFFIC VOLUMES

Future Build condition traffic volumes are derived by adding incremental traffic increases for the project to the 2024 No-Build conditions. Figure 7 present the 2024 Build condition traffic-volume networks for the weekday morning and weekday evening peak hours.

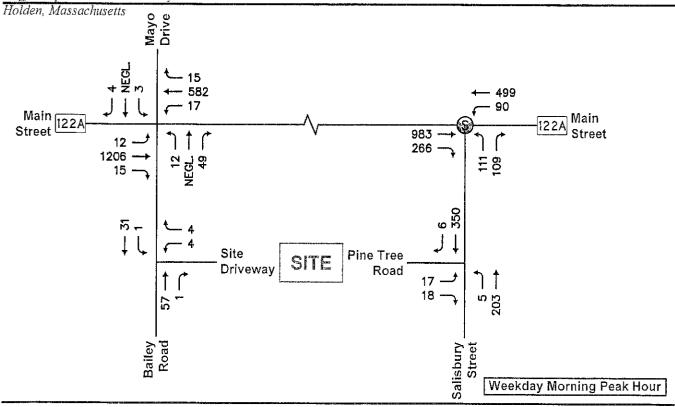


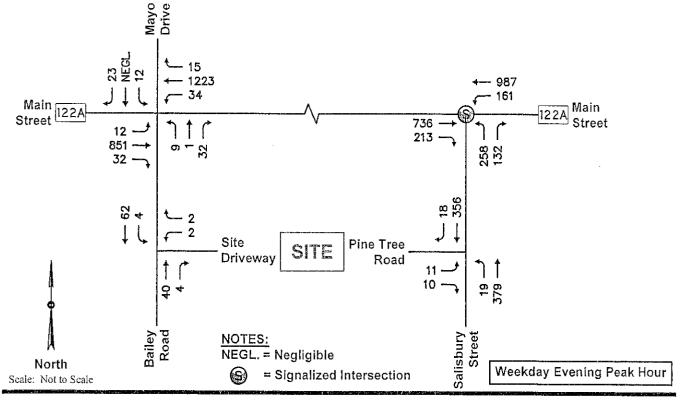


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Figure 6

Site Generated Trips Peak Hour Traffic Volumes





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Figure 7

2024 Build Weekday Peak Hour Traffic Volumes Intersection capacity analyses are presented in this section for the Existing, No-Build, and Build traffic-volume conditions. Capacity analyses, conducted in accordance with EOEEA/EOT guidelines, provide an index of how well the roadway facilities serve the traffic demands placed upon them. The operational results provide the basis for recommended access and roadway improvements in the following section.

4.1 CAPACITY ANALYSIS PROCEDURES

Capacity analysis of intersections is developed using the Synchro® computer software, which implements the methods of the 2010 Highway Capacity Manual (HCM). The resulting analysis presents a level-of-service (LOS) designation for individual intersection movements. The LOS is a letter designation that provides a qualitative measure of operating conditions based on several factors including roadway geometry, speeds, ambient traffic volumes, traffic controls, and driver characteristics. Since the LOS of a traffic facility is a function of the traffic flows placed upon it, such a facility may operate at a wide range of LOS, depending on the time of day, day of week, or period of year. A range of six levels of service are defined on the basis of average delay, ranging from LOS A (the least delay) to LOS F (delays greater than 50 seconds for unsignalized movements and 80 seconds for signalized movements). The specific control delays and associated LOS designations are presented in the Appendix.

4.2 INTERSECTION CAPACITY ANALYSIS RESULTS

Capacity analysis results for the weekday morning and weekday evening peak hour capacity analysis results for the study intersections are described below, with detailed analysis results presented in the **Appendix**.

4.2.1 Level of Service Analysis

Level-of-Service (LOS) analyses were conducted for the Existing (Baseline), No-Build, and Build conditions for the study intersections. The results of the intersection capacity analyses for the unsignalized intersections are summarized below in **Table 7** and **Table 8** for the weekday morning and weekday evening peak hours, respectively. Detailed analysis results are presented in the **Appendix**.

TABLE 7
INTERSECTION CAPACITY ANALYSIS RESULTS
WEEKDAY MORNING PEAK HOUR

		2	019 Baselir	1e	2	024 No-Bu	ild		2024 Builc	l
Location	Approach	v/c1	Delay ²	LOS ³	v/c	Delay	LOS	v/c	Delay	LOS
Salisbury Street at	Eastbound	0.01	11	В	0.01	11	В	0.01	12	В
Pine Tree Road	Northbound	0.00	<5	Α	0.00	<5	Α	0.01	<5	Ā
Bailey Road at	Westbound	n/a4	n/a	n/a	n/a	n/a	n/a	0.01	9	А
Proposed Site Drive	Southbound	n/a	n/a	n/a	n/a	n/a	n/a	0.00	<5	A
Main Street (Route 122A)	Eastbound	0.01	<5	A	0.01	<5	А	0.01	<5	Α
at Bailey Road	Westbound	0.04	<5	Α	0.04	<5	A	0.04	<5	A
	Northbound	>1.0	>50	F	>1.0	>50	F	>1.0	>50	F
	Southbound	0.07	42	E	0.08	46	Е	0.08	48	E
Main Street (Route 122A)	Eastbound	0.88	19	В	0.89	20	В	0.93	25	С
at Salisbury Street	Westbound	0.53	<5	Α	0.54	<5	В	0.56	<5	A
	Northbound	0.23	<u>29</u>	<u>C</u>	0.24	29	<u></u>	0.26	<u>29</u>	<u>C</u>
	Overall	0.88	16	В	0.89	<u></u> 17	B	0.89	19	В

¹Volume-to-capacity ratio

²Average control delay per vehicle (in seconds)

³Level of service

⁴n/a = not applicable

TABLE 8
INTERSECTION CAPACITY ANALYSIS RESULTS
WEEKDAY EVENING PEAK HOUR

		2	019 Baselir	ıe	2	024 No-Bui	ild		2024 Build	1
Location	Approach	v/c¹	Delay²	LOS ³	v/c	Delay	LOS	v/c	Delay	LOS
Salisbury Street at	Eastbound	0.00	15	В	0.00	15	В	0.02	14	В
Pine Tree Road	Northbound	0.00	<5	Α	0.00	<5	Ā	0.05	<5	A
Bailey Road at	Westbound	n/a4	n/a	n/a	n/a	n/a	n/a	0.01	9	Α
Proposed Site Drive	Southbound	n/a	n/a	n/a	n/a	n/a	n/a	0.00	<5	A
Main Street (Route 122A)	Eastbound	0.02	<5	Α	0.02	<5	А	0.02	<5	Α
at Bailey Road	Westbound	0.05	<5	Α	0.05	<5	Α	0.05	<5	A
	Northbound	>1.0	>50	F	>1.0	>50	F	>1.0	>50	F
	Southbound	0.36	>50	F	0.39	>50	F	0.40	>50	F
Main Street (Route 122A)	Eastbound	0.79	16	В	0.80	17	В	0.80	17	В
at Salisbury Street	Westbound	0.78	11	В	0.82	12	В	0.85	14	В
	Northbound	0.19	<u>32</u>	<u>C</u>	0.19	<u>33</u>	<u>C</u>	0.20	<u>33</u>	C
	Overall	0.79	16	В	0.82	17	B	0.85	18	В

¹Volume-to-capacity ratio

As shown in Table 7 and Table 8:

- Operations at the proposed Site Drive intersections with Salisbury Street and Bailey Road are level-of-service (LOS) B or better during the critical peak traffic hours with only minor delays.
- The proposed development is expected to have no material change in delays at study area intersections. Operations at the signalized Main Street at Salisbury Street intersection are projected to be LOS C or better during peak hours with an overall increase in delay of 3 seconds due to the project traffic.
- The minor street approaches at the intersection of Main Street (Route 122A) and Bailey Road/ Mayo Drive currently operate with long delays during the peak hours. Likewise, left turns from Main Street (again low volumes) experience delays, resulting in use of the paved shoulders to by-pass left turning vehicles.

In summary, the proposed development is expected to have a minimal impact on the study area intersections as there will be minimal change in level of service and operations of the study intersections under future conditions as a result of development. Adequate capacity is available under future Build conditions on both Salisbury Street and Bailey Road to accommodate the site use.

22

²Average control delay per vehicle (in seconds)

³Level of service

⁴n/a = not applicable

This section addresses the proposed dimensioning (width) of Pine Tree Road and the other subdivision roadways relative to zoning bylaw requirements and guidelines published by the American Association of State Highway and Transportation Officials (AASHTO). Pine Tree Road is defined as a "way in existence" and will serve as the primary means of access/egress for the proposed subdivision and is proposed as a 24-foot wide subdivision roadway with a grass strip and sidewalk along the northern edge. It is the opinion of MDM that the proposed 24-foot roadway width for is appropriate for Pine Tree Road based on review of AASHTO recommended practice and guidance provided by the Institute of Transportation Engineers (ITE) and Urban Land Institute (ULI) for low volume local residential streets. This design width will also result in less environmental impact (impervious area and associated drainage runoff) and will encourage lower travel speeds that are in keeping with the residential nature of the proposed subdivision. Specific discussion of design criteria leading to this conclusion is presented below.

5.1 Roadway Classification and Design Criteria

A nominal roadway width of 28 feet is required under local zoning by-laws for a local subdivision roadway, requiring a dimensional waiver for the proposed narrower roadway width. The requested waiver (reduced roadway width) is purposely intended to avoid "over designing" the subdivision roadway and encouraging lower travel speeds that are in keeping with lower volume local residential streets. As Pine Tree Road will primarily carry traffic associated with the development and occasional service/emergency vehicles and visitor traffic, projected daily traffic volume is generally less than 700 vehicles per day (vpd).

The Urban Land Institute (ULI), American Society of Civil Engineers (ASCE) and Institute of Transportation Engineers (ITE) together have developed residential street design criteria as published in *Residential Streets, Third Edition*³. *Residential Streets* recommends that local streets, regardless of their average daily traffic volume, be designed for low vehicle speeds, that is, a speed of 15 to 20 miles per hour. *Residential Streets* acknowledges that overly designed streets with an undue concern with geometry more appropriate for highways encourages greater travel speeds and therefore, should be avoided. The American Association of State Highway and Transportation Officials' (AASHTO) "Green Book"⁴ also provides specific design criteria for local low volume roads. Evaluation of the Pine Tree Road's alignment was applied in accordance with AASHTO guidelines for this roadway type, specifically roadway width.

Roadway Width

AASHTO guidance suggests various roadway and a graded shoulder width for new construction of local roads based on design speed and design volume (vehicles per day). The minimum recommended roadway design widths for the proposed Salisbury Pine Tree Estates subdivision for design speeds of 30 mph or less are summarized in Table 9.

TABLE 9
SUMMARY OF ROADWAY DESIGN WIDTHS

		AASHTO Reco	mmended
Roadway Segment	Estimated ADT¹	Travel Width ²	Shoulder Width ³
Roadway 1 (Henry Way)	200±	18	2
Roadway 2 (Farmers Way)	500±	20	3
Pine Tree Road	600±	20	3

Source: AASHTO 2018

As summarized in Table 9:

□ Pine Tree Road: The AASHTO design criteria for Pine Tree Road is a minimum travel width of 20 feet and a graded shoulder width of 3 feet on each side of the roadway. The design width of 24 feet for Pine Tree Road (a way in existence) and associated 5 to 8-foot side grass strips along the road will satisfy the AASHTO recommended minimum roadway width criteria.

¹Estimated average daily traffic in vehicles per day (vpd) based on average trip distribution patterns.

²Minimum width of traveled way (feet) for specific design volume (vehicles/day) and design speed ≤30 mph.

³Width of graded shoulder on each side of the road (feet).

³Residential Streets, Third Edition, published by Urban Land Institute; Washington, D.C., 2001.

⁴A Policy on Geometric Design of Highways and Streets, American Association of State Highway and Transportation Officials (AASHTO), 2018.

□ Subdivision Roadways: Henry Road has projected roadway volumes that classify these roadways as very low volume local roadways following AASHTO guidance (ADT ≤400 vehicle per day). Under this classification, minimum recommended roadway width is 18 feet and a graded shoulder width of 2 feet on each side of the roadway. The AASHTO design criteria for the Farmers Way is a minimum travel width of 20 feet and a graded shoulder width of 3 feet on each side of the roadway. While the subdivision roadways have been designed to comply with the local subdivision regulations which indicate a 28 foot paved width, it is the Applicant's desire is to reduce the pavement width for these two roads to match the proposed Pine Tree Road pavement width of 24 feet – a width that exceeds recommended AASHTO criteria.

A consistent subdivision roadway width of 24 feet would minimize impervious area, provide consistency with Pine Tree Road, encourage lower travel speeds that are in keeping with the residential nature of the proposed subdivision and local roadway system, and is consistent with AASHTO recommended roadway widths for low volume local roadways.

Additional measures to encourage lower travel speeds (particularly along Pine Tree Road), may include posting of speed limit signs (15 mph) and speed "humps" or "tables" at strategic locations. The use of any such measures should be designed to complement the physical alignment of the roadway to ensure that travel within the development is in harmony with the development's design intent.

6.1 RECOMMENDATIONS

MDM finds that travel conditions in the site vicinity along Salisbury Street and Bailey Street are generally unconstrained. Trip generation for the development is estimated at approximately 52 vehicle-trips during the weekday morning peak hour and 66 vehicle-trips during the weekday evening peak hour. Traffic impacts associated with the residential development are not expected to notably affect travel or safety conditions in the site vicinity. However, MDM recommends access-related improvements aimed at enhancing traffic operations and/or travel safety. Specific recommendations are as follows:

Pine Tree Road at Salisbury Street. The existing Pine Tree Road and Salisbury Street intersection will serve as primary access to the site. Currently, no traffic control or marked pedestrian crossing is present on the Pine Tree Road eastbound approach. MDM recommends the following improvements:

- □ A STOP sign (R1-1) and STOP line pavement markings is recommended on the Pine Tree Road approach to Salisbury Street. A marked crosswalk and ADA compliant ramps should be installed at the intersection across Pine Tree Road.
- A sidewalk is recommended on Pine Tree Road to connect the site with the existing sidewalk system on the western side of Salisbury Street which extends from Main Street to the Dawson Elementary School.
- □ Plantings (shrubs, bushes) and structures (walls, fences, etc.) should be maintained at a height of 2 feet or less within the Salisbury Street layout in vicinity of the site driveway to provide unobstructed sight lines.

Bailey Road at Proposed Site Drive. The proposed site driveway will connect the site with Bailey Road just south of the existing garage for #124 Bailey Road. MDM recommends that the Applicant implement the following items:

- □ A STOP sign (R1-1) and STOP line pavement markings should be installed on the Site Drive approach to Bailey Road.
- □ Plantings (shrubs, bushes) and structures (walls, fences, etc.) should be maintained at a height of 2 feet or less within the Bailey Road layout in vicinity of the site driveway to provide unobstructed sight lines.

6.2 CONCLUSIONS

Adequate capacity is available under future Build conditions on both Salisbury Street and Bailey Road to accommodate the site use. The project is not projected to significantly change any reported operating levels compared to future No-Build conditions. Proposed access improvements will provide ample capacity to accommodate site-generated traffic while also enhancing safety and capacity.

APPENDIX

- □ Traffic Volume Data
- ☐ Seasonal/Yearly Growth Data
- □ Speed Data
- □ Crash Data
- ☐ Sight Distance Calculations
- □ Trip Generation
- ☐ Trip Distribution Calculations
- □ Capacity Analysis



N/S: Salisbury Street North of Site Driveway Holden, MA

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N/S: Bailey Road North of Thorny Lea Road Holden, MA

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11:30 11:45	un nun munde i Grijanski se se se	8 5	2	23		1945 14 - 14 3 1945 1941 - 14 3	0		70° - 30° 3 °	58	lendavis (6)
Total	er ser en tymperisch	185	264		. r.j.r.thair. 3	200		1		385	693
Percent		41.2%	58.8%			31.8%				35.7%	64.3%
Combined										107	
Total		4	49				629				3
											

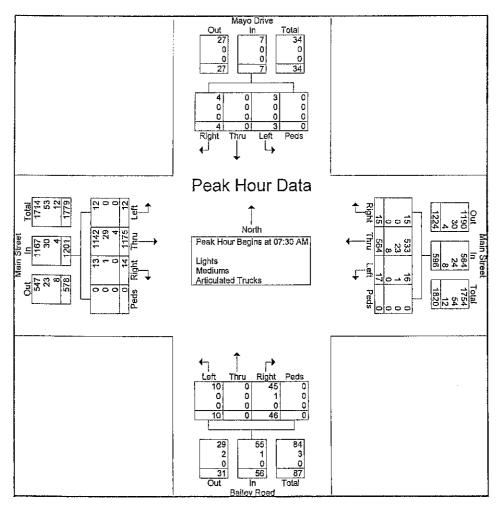
E/W: Main Street NB: Bailey Road SB: Mayo Drive

Holden, MA

File Name: 435 Main St Bailey Rd 5-7-19

Site Code: 435 Start Date : 5/7/2019

			ayo D					ain St					iley R		·····			ain St			
								rom E				- 17	om So				r				
Start Time		Thru			App. Total	Right	Thru		Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App, Total	Int. Total
Peak Hour A	Analysi	s Fron	n 07:0	O AM t	o 11:45	AM -	Peak	1 of 1													
Peak Hour fo	or Enti	re Inte	rsectio	on Beg	ins at 0	7:30 A	M														
07:30 AM	0	0	1	0	1	4	106	1	0	111	10	0	2	0	12	5	310	4	0	319	443
07:45 AM	1	0	0	0	1	5	151	4	0	160	7	0	5	0	12	2	287	3	0	292	465
08:00 AM	1	0	2	0	3	2	175	3	0	180	15	0	1	0	16	6	303	4	0	313	512
08:15 AM	2	0	0	0	2	4	132	9	0	145	14	0	2	0	16	1	275	1	0	277	440
Total Volume	4	0	3	0	7	15	564	17	0	596	46	0	10	0	56	14	1175	12	0	1201	1860
% App. Total	57.1	0	42.9	0		2.5	94.6	2.9	0		82.1	0	17.9	0		1.2	97.8	1	0		
PHF	.500	.000	.375	.000	.583	.750	806	.472	.000	.828	.767	.000	,500	.000	.875	.583	.948	.750_	.000	.941	.908
Lights	4	0	3	0	7	15	533	16	0	564	45	0	10	Q	55	13	1142				
% Lights	100	0	100	0	100	100	94,5	94.1	0	94.6	97.8	0	100	0	98.2	92.9	97.2	100	0	97.2	96,4
Mediums	0	0	0	0	0	0	23	1	0	24	1	0	0	0	1	1	29	0	0	30	55
% Mediums																					
Articulated Trucks	0	0	0	0	0	0	8	0	0	8	0	0	0	0	0	0	4	0	0	4	12
% Articulated Trucks	0	0	0	0	0	0	1.4	0	0	1,3	0	0	0	0	0	0	0.3	0	0	0,3	0.6



MDM Transportation Consultants, Inc. 28 Lord Road, Suite 280

Marlborough, MA

E/W: Main Street NB: Bailey Road

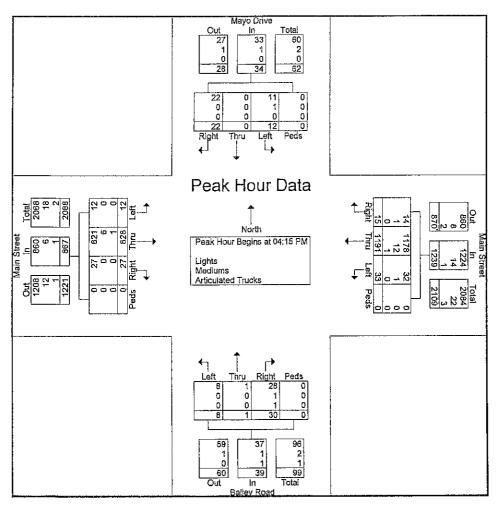
SB: Mayo Drive Holden, MA

File Name: 435 Main St Bailey Rd 5-7-19

Site Code: 435

Start Date : 5/7/2019

			layo D				M	ain St	reet				iley R					ain St		-	
		F.	rom No	orth			F	rom E	ast			Fr	om Sc	outh			Fi	om W			
Start Time	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Right	Thru	Left	Peds	App. Total	Rìght	Thru	Left	Peds	App. Total	Int. Total
Peak Hour A	nalys!	s Fror	n 12:0	0 PM to	05:45	PM -	Peak '	1 of 1													
Peak Hour fe	or Enti	re Inte	rsection	on Beg	ins at 0	4:15 F	ľΜ														
04:15 PM	9	0	5	0	14	7	302	6	0	315	7	0	2	0	9	6	217	1	0	224	562
04:30 PM	1	0	1	0	2	1	295	9	0	305	8	0	3	0	11	8	199	4	0	211	529
04:45 PM	6	0	4	0	10	2	284	10	0	296	7	1	3	0	11	8	206	3	0	217	534
05:00 PM	6	0	2	0	8	5	310	8	0	323	8	0	0	0	8	5	206	4	0	215	554
Total Volume	22	0	12	0	34	15	1191	33	0	1239	30	1	8	0	39	27	828	12	0	867	2179
% App. Total	64.7	0	35.3	0		1.2	96.1	2.7	0		76.9	2.6	20.5	0		3.1	95.5	1.4	0		
PHF	.611	.000	.600	.000	.607	.536	.960	.825	.000	.959	.938	.250	.667	.000	.886	.844	.954	.750	.000	.968	,969
Lights	22	0	11	0	33	14	1178			·											
% Lights	100	0	91.7	0	97.1	93.3	98.9	97.0	0	98.8	93.3	100	100	0	94.9	100	99,2	100	0	99.2	98.9
Mediums	0	0	1	0	1	1	12	1	0	14	1	0	0	0	1	0	6	0	0	6	22
% Mediums																			_		
Articulated Trucks	0	٥	0	0	0	0	1	0	0	1	1	0	0	0	1	0	_ 1	0	0	1	3
% Articulated Trucks	0	0	0	0	0	0	0.1	0	0	0.1	3.3	0	0	0	2.6	0	0.1	0	0	0.1	0.1



E/W: Main Street NB: Bailey Road

SB: Mayo Drive Holden, MA

File Name: 435 Main St Bailey Rd 5-7-19

Site Code: 435 Start Date : 5/7/2019

Groups Printed- Lights - Med	nums - Articulated Trucks
Main Street	Bailey Road

	1	N	layo Di	rive		<u> </u>		ain St			1101119		iley R	oad			M	ain St	reet		
			rom No		i			rom E					om So			}	F	rom W	/est		
Start Time	Right	Thru	Left		App. Total	Right	Thru	Left		App. Total	Right	Thru		Peds	App. Total	Right	Thru	Left	Peds	App. Total	Int. Total
07:00 AM	1	2	5	0	8	6	164	2	0,	172	10	0	3	0	13	3	275	3	0	281	474
07:15 AM	1	0	1	0	2	6	116	1	0	123	9	1	3	0	13	2	244	2	0	248	386
07:30 AM	0	0	1	0	1	4	106	1	0	111	10	0	2	0	12	5	310	4	0	319	443
07:45 AM	1	0	0	0	1	5	151	4	0	160	7	0	5	0	12	2	287	3	0	292	465
Total	3	2	7	0	12	21	537	8	0	566	36	1	13	0	50	12	1116	12	0	1140	1768
08:00 AM	1 1	0	2	0	3	2	175	3	0	180	15	0	1	0	16	6	303	4	٥	313	512
08:15 AM	2	Ō	ō	ó	2	4	132	9	ō	145	14	0	2	0	16	1	275	1	0	277	440
08:30 AM	1	ō	4	ō	5	4	133	7	ō	144	7	1	2	0	10	8	252	6	0	266	425
08:45 AM	1	Ō	4	ō	5	4	152	12	Ö	168	11	0	3	0	14	18	252	7	0	277	464
Total	5	0	10	0	15	14	592	31	0	637	47	1	8	0	56	33	1082	18	0	1133	1841
	_	_			1			_	_			_	_		4.5		200			205	
04:00 PM	7	0	4	0	11	7	293	6	0	306	9	0	6	0	15	1	203 217	1	0	205 224	537
04:15 PM	9	0	5	0	14	7	302	6	0	315	7	0	2	0	9 11	6 8	199	1 4	0	211	562
04;30 PM	1	0	1	0	2	1	295	9	0	305	8	0	3	0		8	206	3	0	217	529 534
04:45 PM	6 23	0	4	0	10	2	284	10 31	<u>0</u> _	296	7 31	1	3 14	0	11 46	23	825	9	0	857	2162
Total	23	0	14	U	37	17	1174	31	υ	1222	١٠.	ı	14	U	40	23	020	9	U	607	2102
05:00 PM	6	0	2	0	8]	5	310	8	0	323	8	0	0	0	8	5	206	4	0	215	554
05:15 PM	3	1	2	0	6	3	296	8	0	307	10	0	1	0	11	7	211	0	0	218	542
05:30 PM	5	0	1	0	6	1	277	8	0	286	4	0	3	0	7	7	184	3	0	194	493
05:45 PM	1	1	5	0	7	3	305	10	0	318	10	0	6	0	16	7	175	1	0	183	524
Total	15	2	10	0	27	12	1188	34	0	1234	32	0	10	0	42	26	776	8	0	810	2113
Grand Total	46	4	41	0	91	64	3491	104	0	3659	146	3	45	0	194	94	3799	47	0	3940	7884
Apprch %	50.5	4.4	45.1	ō		1.7	95.4	2.8	0		75.3	1.5	23.2	0		2.4	96.4	1.2	0		
Total %	0.6	0.1	0.5	0	1.2	0.8	44.3	1.3	0	46.4	1.9	0	0.6	O	2.5	1.2	48.2	0.6	0	50	
Lights	45	4	40	0	89	61	3398										3723				
% Lights	97.8	100	97.6	0	97.8	95.3	97.3	97.1	0	97.3	97.9	100	97.8	0	97.9	98.9	98	100	0	98	97.7
Mediums	1	0	1	0	2	3	82	3	0	88	2	Q	1	0	3	1	67	0	0	68	161
% Mediums																					
Articulated Trucks	0	0	0	0	0	0	11	0	0	11	1	0	0	0	1	0	9	0	0	9	21
% Articulated Trucks	0	0	0	0	0	0	0,3	0	0	0.3	0.7	0	0	0	0.5	0	0.2	0	0	0.2	0.3

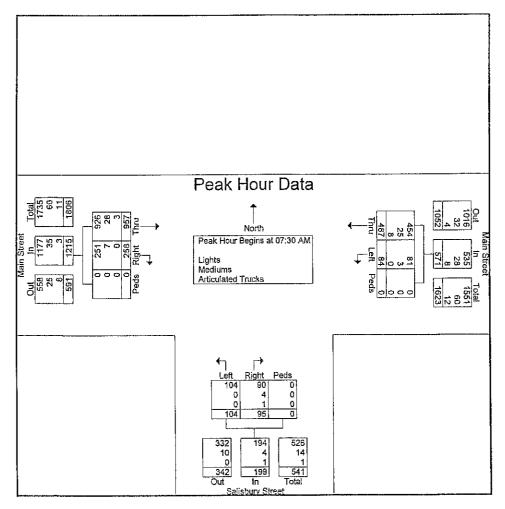
E/W: Main Street NB: Salisbury Street

Holden, MA

File Name: 435 Main Salisbury St 5-7-19

Site Code: 435 Start Date : 5/7/2019

			Street			Salisbu					Street		
		From	East	Į.		From					West		
Start Time	Thru	Left	Peds A	pp. Total	Rìght	Left	Peds	App. Total	Right	Thru	Peds /	App. Total	Int. Total
Peak Hour Analysis					f1								
Peak Hour for Ently	e Intersect	ion Begin	is at 07:30	AM .								1	
07:30 AM	98	15	0	113	23	16	0	39	56	252	0	308	460
07:45 AM	131	21	0	152	21	31	0	52	57	239	0	296	500
08:00 AM	151	27	0	178	25	31	0	56	82	238	0	320	554
08:15 AM	107	21	0	128	26	26	0	52	63	228	0	291	471
Total Volume	487	84	0	571	95	104	0	199	258	957	0	1215	1985
% App. Total	85.3	14.7	0		47.7	52.3	0		21.2	78.8	0		
PHF	.806	.778	.000	.802	.913	.839	.000	.888	.787	.949	.000	.949	.896
Lights	454	81	0	535	90	104	0	194	251	926	0	1177	1906
% Lights	93.2	96.4	0	93.7	94.7	100	0	97.5	97.3	96.8	0	96,9	96,0
Mediums	25	3	0	28	4	0	0	4	7	28	0	35	67
% Mediums	5.1	3.6	0	4.9	4.2	0	0	2.0	2.7	2.9	0	2.9	3.4
Articulated Trucks	8	0	0	8	1	0	0	1 (0	3	0	3	12
% Articulated Trucks	1.6	0	0	1.4	1.1	O	0	0.5	0	0.3	0	0.2	0.6



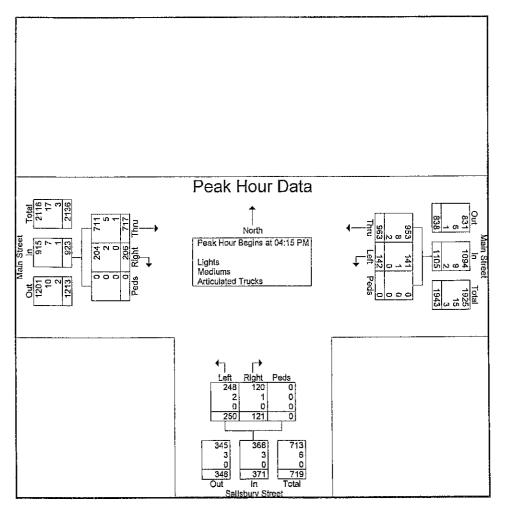
E/W: Main Street NB: Salisbury Street

Holden, MA

File Name: 435 Main Salisbury St 5-7-19

Site Code: 435 Start Date : 5/7/2019

			Street East			Salisbur From				Main From	Street West		
Start Time	Thru	Left	Peds /	pp. Total	Right	Left	Peds	App. Total	Right	Thru	Peds	App. Total	Int. Total
Peak Hour Analysis					of 1								
Peak Hour for Entir	e Intersect	ion Begir	ns at 04:15	PM .									
04:15 PM	248	36	0	284	12	60	0	72	53	210	0	263	619
04:30 PM	241	29	0	270	32	63	0	95	48	175	0	223	588
04:45 PM	224	41	0	265	32	63	0	95	50	181	0	231	591
05:00 PM	250	36	0	286	45	64	0	109	55	151	0	206	601
Total Volume	963	142	0	1105	121	250	0	371	206	717	0	923	2399
% App. Total	87.1	12,9	0		32.6	67.4	0		22.3	77.7	0		
PHF	.963	.866	.000	.966	.672	.977	.000	.851	.936	.854	.000	.877	.969
Lights	953	141	0	1094	120	248	0	368	204	711	0	915	2377
% Lights	99.0	99.3	٥	99.0	99.2	99.2	0	99.2	* 99.0	99,2	0	99,1	99.1
Mediums	8	1	0	9	1	2	0	3	2	5	0	7	19
% Mediums	0,8	0.7	0	0.8	0.8	0,8	٥	0.8	1.0	0.7	0	0.8	0.8
Articulated Trucks	2	0	0	2	0	0	0	0	0	1	0	1	3
% Articulated Trucks	0.2	0	0	0.2	0	0	0	0	0	0.1	0	0,1	0,1



E/W: Main Street NB: Salisbury Street

Holden, MA

File Name: 435 Main Salisbury St 5-7-19

Site Code: 435 Start Date : 5/7/2019

	Groups Printed-	Lights	 Mediums 	- Articulated Trucks
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				Groups Pri	inted- Ligh	nts - Medin	ums - Arti	iculated Tru	ıcks				
		Main	Street			Salisbur	y Street				Street		
		From	East			From	South				West		
Start Time	Thru	Left	Peds	App. Total	Right	Left	Peds	App. Total	Right	Thru	Peds	App. Total	Int. Total
07:00 AM	118	10	0	128	23	45	0	68	49	239	0	288	484
07:15 AM	81	12	0	93	17	33	0	50	43	219	0	262	405
07:30 AM	98	15	0	113	23	16	0	39	56	252	0	308	460
07:45 AM	131	21	0	152	21	31	0	52	57	239	0	296	500
Total	428	58	0	486	84	125	0	209	205	949	0	1154	1849
08:00 AM l	151	27	0	178	25	31	0	56	82	238	0	320	554
08:15 AM	107	21	õ	128	26	26	Ō	52	63	228	0	291	471
08:30 AM	115	27	ŏ	142	20	35	ō	55	54	199	Ó	253	450
08:45 AM	122	23	ō	145	30	49	ō	79	59	210	0	269	493
Total	495	98	0	593	101	141	Ō	242	258	875	0	1133	1968
·													
04:00 PM	254	24	0	278	26	56	0	82	46	173	0	219	579
04:15 PM	248	36	0	284	12	60	0	72	53	210	0	263	619
04:30 PM	241	29	0	270	32	63	0	95	48	175	0	223	588
04:45 PM	224	41	0	265	32	63	0	95	50	181	0	231	591
Total	967	130	0	1097	102	242	0	344	197	739	О	936	2377
05:00 PM	250	36	0	286	45	64	0	109	55	151	0	206	601
05:15 PM	244	17	ō	261	18	60	0	78	40	180	0	220	559
05:30 PM	222	30	Ö	252	21	61	٥	82	47	146	Ö	193	527
05:45 PM	257	35	Ō	292	33	53	0	86	29	156	0	185	563
Total	973	118	0	1091	117	238	0	355	171	633	0	804	2250
Grand Total	2863	404	0	3267	404	746	0	1150 İ	831	3196	0	4027	8444
Approh %	87.6	12.4	ŏ	3207	35.1	64.9	ŏ	1100	20.6	79.4	ŏ		• • • • • • • • • • • • • • • • • • • •
Total %	33.9	4.8	ŏ	38.7	4.8	8.8	õ	13.6	9.8	37.8	ŏ	47.7	
Lights	2784	397	0	3181	393	729	0	1122	812	3132	0	3944	8247
% Lights	97.2	98.3	ŏ	97.4	97.3	97.7	ŏ	97.6	97.7	98	õ	97.9	97.7
Mediums	67	7	0	74	10	17	0	27	19	59	0	78	179
% Mediums	2.3	1.7	ŏ	2.3	2.5	2.3	ō	2.3	2.3	1.8	Ō	1.9	2.1
Articulated Trucks	12	0	0	12	1	0	0	1	0	5	0	5	18
% Articulated Trucks	0.4	0	0	0.4	0.2	0	0	0.1	0	0.2	0	0.1	0.2

☐ Seasonal Data/ Yearly Growth

			:
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			:
			i :

SECTION I - CONTINUOUS COUNTING STATION MONTHLY AVERAGE DAILY TRAFFIC

STATION 3293 - WORCESTER - RTE.I-190 - NORTH OF RTE.12	STER - RTE.I-19	90 - NORTH	OF RTE.12	í,	2	3	;	!					
¥1	JAN	2	MAR	A A	MAY	205	JUL	AUG	SEP	OCT	200	DEC	YEAR
11	30,026	31,649	33,440	32,643	33,279	33,404	31,595	32,277	33,985	34,166	33,039	32,027	32.628
	4%	4%	-5%	3%	1%	1%	3%	2%	%0	%0	%0	-1%	1%
12	31,080	32,917	32,746	33,541	33 556	33,820	32,591	33,055	33,999	34 112	33.038	31 863	700 66
	1%	-8%	-2%	-1%	0%	%0	-3%	%	%	1 %	%0	, .	100,00
13	31,435	30,284	32,046	33,314	33,508	33,923	31,678	33,489	34 412	34.600	32.881	29 968	32.628
	4%	1%	3%	1%	2%	4%	89	4%	-2%	1%	-2%	5%	26
14	30,187	30,538	33,054	33,676	34,126	35,189	33,547	34,820	33,774	35.007	32 326	31.463	33.142
	%0	2%	1%	3%	3%	3%	3%	3%	4%	4%	%9	4%	3%
17	30,278	32,762	34,539	36,645	37,243	38,257	36,152	37,974	38,157	39,047	38,345	35,181	36,215
Seasonal Adjustment Factor	1.10	1.06	1.01	56.0	0.98	0.96	1.01	0.98	0.96	0.95	0.99	1.05	
(to average month)												Growth	1.17%
	STATION 307 - WEST		BOROUGH - RTE.9	-EAST OF	- EAST OF NORTHBOROUGH T.	JUGH T.L.							
ΥR	JAN		MAR	APR	MAY	NO.	JUL	AUG	SEP	TOO) 2	Ü	Q LL V
07	47,505	47,283	49,268	49,136	50,000	52,000	53,000	52,322	49,031	50.571	49.662	47,007	49.732
	~4%	-2%	-3%	1%	1%	-4%	~8%	-1%	-1%	3%	4%	-1%	3%
80	45,614	46,112	47,829	49,816	50,518	49,936	48,629	48,759	48,531	49 009	47,490	46.596	48.245
	3%	1%	%;	-2%	-2%	%0	-2%	-3%	-2%	-1%	%0	5%	-1%
60	44,103	46,434	46,455	49,049	49,474	49,934	47,638	47,056	47,762	48,663	47,379	47,564	47,626
,	%:!	%0	%	%0	%0	1%	-1%	1%	1%	1%	2%	2%	1%
	43,244	45,150	48,016	48,943	49.781	50,525	46,812	48,234	48,825	49,198	49,151	49,888	48,231
Ç	%)	%2.5	%	-1%	1%	%	%	4%	%0	2%	2%	-5%	%
7.5	46,381	46,683	48,608	48,662	50,126	49,961	48,380	49,941	48,882	50,056	50,015	47,600	48,791
	%0	-1%	-2%	*	%	% o -	3%	%"	2%	%0	-1% -1%	2%	%0
13	46,393	46,220	47,421	49,359	50,657	45,623	49,797	49,223	49,935	50,021	49,651	48,441	48,562
Seasonal Adjustment Factor	1.07	1.04	1.01	0.99	0.97	0.98	66'0	0.99	0.99	0.98	66.0	1.01	
(to average month)											Ö	Growth	-0.65%
STATION 3140 - PAXTON - PLEASANT STREET - NORTH OF TURKEY HILL BROOK BRIDGE	PLEASANT ST	REET - NOR	TH OF TURKE	EY HILL BRC	OK BRIDGE								
YR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	>0N	CHC	YEAR
17	4,280	4,287	4,496	4,935	5,187	5,328	5,246	5,266	5,147	5,144	4.740	4.394	4 871
Seasonal Adjustment Factor	1.14	1.14	1.08	0.99	0.94	0.91	0.93	0.92	0.95	0.95	1.03	1.11	
(to average month)													
Average	JAN	FEB	MAR	APR	MAY	NUS	JIC.	AUG	SEP	OCT	NOV	DEC	
Seasonal Adjustment Factor (to average month)	1.10	1.08	1.04	0.99	0.96	0.95	0.98	96.0	0.97	0.96	1.00	1.06	
francis official orl													

Average Yearly Growth Calculated 0.26* Yearly Growth Pactor Used 0.5%

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□ Speed Data

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MDM TRANSPORTATION CONSULTANTS, INC. 28 Lord Road, Suite 280 Marlborough, MA

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28 Lord Road, Suite 280	Marlborough, MA www.mdmtrans.com	46	5 5	3	0	0	0	0	0	0	7	0	0	0	0	0	0	0	0	-	0	0	0	0	0	0	0	က
3 Lord Roa	Marlborough, MA ww.mdmtrans.c	41	45	0	0	0	0	Φ	0	0	7	0	0	0	0	0	0	0	0	0	7	0	-	-	_	0	0	7
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	ea Road	1	15	0	0	0	0	-	0	4	0	0	0	4	0	0	γ	-	n	0	,	τ	0	0	τ	0	0	17
N/S: Bailey Road	North of Thorny Lea Road Holden, MA	Northbound	Time	05/07/19	01:00	02:00	03:00	04:00	02:00	00:90	07:00	08:00	00:60	10:00	11:00	12 PM	13:00	14:00	15:00	16:00	17:00	18:00	19:00	20:00	21:00	22:00	23:00	Total

22 MPH 15th Percentile:

Percentil

35 MPH 39 MPH 85th Percentile: 95th Percentile: 30 MPH 26-35 MPH 63.3% 284 358 79.7% Mean Speed(Average):
10 MPH Pace Speed:
Percent in Pace:
Number of Vehicles > 25 MPH:
Percent of Vehicles > 25 MPH:

Statistics

		ulca	Percent		*	*	29	37	38	38	36	34	34	35	34	37	33	35	34	34	37	33	34	34	33	52	39		
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Lord Road, Suite 28 Marlborough, MA w.mdmtrans.co	46	0 0	200	0 0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
28 Lord Road, Suite 280 Marlborough, MA www.mdmtrans.com	41	4	7	0 0	Э,	0	0	0	0	7	-	0	-	0	0	0	0	0	-	0	0	0	0	0	0	0	0	2	
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N/S: Bailey Road North of Thorny Lea Road Holden, MA	Northbound	Limo	05/08/19	00:50	00:10	02:00	03:00	04:00	02:00	00:90	00:20	08:00	00:60	10:00	11:00	12 PM	13:00	14:00	15:00	16:00	17:00	18:00	19:00	20:00	21:00	22:00	23:00	Total	Percentii es

30 MPH 26-35 MPH 64.5% 284 353 80.2%

Mean Speed(Average):
10 MPH Pace Speed:
Percent in Pace:
Number of Vehicles > 25 MPH:
Percent of Vehicles > 25 MPH:

Statistics

35 MPH 38 MPH

85th Percentile: 95th Percentile:

MDM TRANSPORTATION CONSULTANTS, INC.

28 Lord Road, Suite 280 Marlborough, MA

N/S: Bailey Road North of Thorny Lea Road

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Holden MA	Northbound	Start	Time	05/09/19	01:00	02:00	03:00	04:00	02:00	00:90	02:00	08:00	00:60	10:00	11:00	12 PM	13:00	14:00	15:00	16:00	17:00	18:00	19:00	20:00	21:00	22:00	23:00	Total	

36 MPH 39 MPH

85th Percentile: 95th Percentile:

23 MPH

15th Percentile:

Percentil

30 MPH 26-35 MPH

64.3% 292 378 83.3%

Mean Speed(Average):
10 MPH Pace Speed:
Percent in Pace:
Number of Vehicles > 25 MPH:
Percent of Vehicles > 25 MPH:

Statistics

22 MPH 30 MPH 35 MPH 39 MPH

15th Percentile: 50th Percentile: 85th Percentile: 95th Percentile:

Summary

30 MPH

Mean Speed(Average):

Statistics

30 MPH 26-35 MPH 63.6% 400 507 80.6%

Mean Speed(Average):
10 MPH Pace Speed:
Percent in Pace:
Number of Vehicles > 25 MPH:
Percent of Vehicles > 25 MPH:

Statistics

35 MPH 39 MPH

85th Percentile: 95th Percentile:

15th Percentile:

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MDM TRANSPORTATION CONSULTANTS, INC. 28 Lord Road, Suite 280 Marlborough, MA

,			85th	Percent	*	*	*	*	*	38	37	333	36	37	32	37	35	, co	8 &	38	37	37	. e	37	33	800	36	41		
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			71	75	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	c	0	C	0	· C	0	0	
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N/S: Bailey Road	North of Thorny Lea Road Holden MA	Southbound	Start	Time	05/08/19	00,100	02:00	03:00	04:00	02:00	00:00	02:00	08:00	00:60	10:00	11:00	12 PM	13:00	14:00	15:00	16:00	17:00	18:00	19:00	20:00	21:00	22:00	23:00	Total	

31 MPH 26-35 MPH 62.6% 389 518 83.4%

Mean Speed(Average):
10 MPH Pace Speed:
Percent in Pace:
Number of Vehicles > 25 MPH:
Percent of Vehicles > 25 MPH:

Statistics

36 MPH 39 MPH

85th Percentile: 95th Percentile:

24 MPH

15th Percentile:

Percentil

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	61	65	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
	56	90	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
80 m	51	55	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
28 Lord Road, Suite 280 Marlborough, MA www.mdmtrans.com	46	50	0	o	0	0	0	0	0	0	0	0	0	0	0	0	0	ო	~	0	0	0	0	0	0	0	4		
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N/S: Bailey Road North of Thorny Lea Road Holden, MA Southbound	Start	Time	05/09/19	01:00	02:00	03:00	04:00	02:00	00:90	00:20	08:00	00:60	10:00	11:00	12 PM	13:00	14:00	15:00	16:00	17:00	18:00	19:00	20:00	21:00	22:00	23:00	Total	Percentil es	

30 MPH 26-35 MPH 64.6% 392 505 83.2%

Mean Speed(Average):
10 MPH Pace Speed:
Percent in Pace:
Number of Vehicles > 25 MPH:
Percent of Vehicles > 25 MPH:

Statistics

23 MPH 30 MPH 36 MPH 39 MPH

15th Percentile : 50th Percentile : 85th Percentile : 95th Percentile :

Summary

30 MPH

Mean Speed(Average):

Statistics

28 Lord Road, Suite 280 Marlborough, MA www.mdmtrans.com	46 51 56 61 66 71	55 60 65 70 75 999 Total Pe	0 0 0				0		0 0 0	0 0 0 0 0 0 0 214	0 0 0 0 0 0 0 0 598	0 0 0 0 0 0 0 212	0 0 0 0 0	0 0 0 0 182	0 0 0 0 158	021 6 6 6 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0	0 0 0 0 0 0 0 569 31	0 0 0 0 0 0 0 0 5	0 0 0 0 0 0 0 135	0 0 0 0 0 0 110	0 0 0 0 0 83	0 0 0 0 0 0 43	0 1 0 0 0 0 1 24	0 1 3098		
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	26	30	-	0	0	0	7	14	46	96	135	88	71	80	73	91	76	108	118	128	85	61	25	42	19	-	1397		i co
	21	25	0	0	0	0	0	თ	26	46	69	57	35	42	34	સ	59	49	83	58	43	32	22	23	16	S	748	15th Percentile :	85th Percentile ;
veway	16	20	0	0	_	-	τ-	0	4	2	4	4	ဖ	5	7	4	9	10	13	11	m	7	ო	-	0	0	93	15th	85#
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N/S: Salisbury Street North of Proposed Site Driveway Holden, MA Southbound	Start	me	05/07/19	04:00	02:00	03:00	04:00	02:00	06:00	00:20	08:00	00:60	10:00	11:00	12 PM	13:00	14:00	15:00	16:00	17:00	18:00	19:00	20:00	21:00	22:00	23:00	Total	Percentil es	

27 MPH 21-30 MPH 69.3% 2145 104 3.4%

Mean Speed(Average):
10 MPH Pace Speed:
Percent in Pace:
Number of Vehicles > 35 MPH:
Percent of Vehicles > 35 MPH:

Statistics

	85th	Percent	35	29	29	24	34	33	33	32	31	31	32	31	31	31	32	31	29	32	31	32	31	31	30	32	
		Total	9	ო	-	2	7	28	106	205	304	185	157	144	157	167	198	218	291	274	215	175	137	93	43	30	3146
	76	666	0	0	0	0	0	0	0	0	0	0	o	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	71	75	0	D	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
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	61	65	0	0	0	0	0	0	0	0	0	a	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	56	90	0	0	0	0	0	0	0	0	0	0	O	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30 m	51	55	0	0	0	0	0	0	0	0	0	0	0	0	O	0	0	0	0	0	0	0	0	0	0	0	0
Lord Road, Suite 28 Marlborough, MA w.mdmtrans.co	46	20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	-	D	0	0	0	0	0	0	0	
28 Lord Road, Suite 280 Mariborough, MA www.mdmtrans.com	41	45	0	0	0	0	0	0	0	1	γ	-	0	0	0	0	0	0	0	₩.	0	0	-	0	0	0	5
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	31	35		0	0	0	က	ო	5	47	56	31	33	27	28	39	45	38	27	53	41	38	23	8	ø	∞	585
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eet I Site Drive.	-	15	0	0	0	0	0	2	۸	ထ	1,4	7	2	4	10	70	4	80	9	&	11	7	က	က	7	0	108
N/S: Salisbury Street North of Proposed Site Driveway Holden, MA Southbound	Start	Time	05/08/19	01:00	02:00	03:00	04:00	05:00	00:90	02:00	08:00	00:60	10:00	11:00	12 PM	13:00	14:00	15:00	16:00	17:00	18:00	19:00	20:00	21:00	22:00	23:00	Total

27 MPH 21-30 MPH 71.6% 2254 100 3.2%

Mean Speed(Average):
10 MPH Pace Speed:
Percent in Pace:
Number of Vehicles > 35 MPH:
Percent of Vehicles > 35 MPH:

Statistics

21 MPH

15th Percentile:

Percentil

31 MPH 34 MPH

85th Percentile: 95th Percentile:

N/S: Salisbury Street	Street) }	28 Lord Ro	28 Lord Road, Suite 280)))))
Holden, MA Southbound		liveway				•	www.mdr	www.mdmtrans.com	ш							
Start	4- K	16	21	26	34	98	41	46	51	56	61	99	7.1	76		85th
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Percentil es		15th F	15th Percentile:	21	21 MPH											
		85th F 95th F	85th Percentile : 95th Percentile :	34	31 MPH 34 MPH											
Statistics	Number Percent	Mean Speed(Average) 10 MPH Pace Speed Percent in Pace Number in Pace Number of Vehicles > 35 MPH Percent of Vehicles > 35 MPH	Speed(Average): IPH Pace Speed: Percent in Pace: Number in Pace: ides > 35 MPH: ides > 35 MPH:	27 MPH 21-30 MPH 72.7% 2336 109	27 MPH 30 MPH 72.7% 2336 109 3.4%											

21 MPH 26 MPH 31 MPH 34 MPH

15th Percentile : 50th Percentile : 85th Percentile : 95th Percentile :

Summary

27 MPH

Mean Speed(Average):

Statistics

N/S: Salisbury Street North of Proposed Site Driveway Holden, MA Northbound

85th	Percent	34	32	34	37	37	35	35	34	33	33	¥	34	34	35	33	33	15	32	34	34	34	34	34	37	
	Total	6	4	-	4	14	37	66	210	211	228	218	198	202	180	227	272	163	276	272	171	108	69	29	14	3216
76	666	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
71	75	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
99	20	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
51	65	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
56	90	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
51	55	0	0	0	0	0	0	0	0	0	0	0	0	o	0	0	0	0	0	0	0	0	0	0	0	0
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26	30	3	2	0	က	4	8	21	83	89	100	88	74	83	58	26	104	0	75	90	48	45	29	10	7	1115
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+	15	0	0	o	0	, -	0	2	ო	ស	2	4	23	ы	7	5	18	138	93	15	4	4	-	7	0	304
Start	Time	05/07/19	01:00	02:00	03:00	04:00	02:00	00:90	00:20	08:00	00:60	10:00	11:00	12 PM	13:00	14:00	15:00	16:00	17:00	18:00	19:00	20:00	21:00	22:00	23:00	Total

22 MPH 15th Percentile: Percentil

34 MPH 37 MPH 85th Percentile: 95th Percentile:

Statistics

28 MPH 26-35 MPH 71.0% 2284 300 9.3%

Mean Speed(Average):
10 MPH Pace Speed:
Percent in Pace:
Number of Vehicles > 35 MPH:
Percent of Vehicles > 35 MPH:

N/S: Salisbury Street	Street) : :	28 Lord Rc	28 Lord Road, Suite 280	280							,
North of Proposed Site Driveway Holden, MA	osed Site Dri	iveway					Mariboi www.mdi	Mariborough, MA www.mdmtrans.com	mc							
Northbound						İ										
Start	τ-	16	74	56	31	36	4-	46	51	56	61	99	71	76		85th
Time	15	20	25	30	35	40	45	20	55	90	65	202	7.5	555	Total	Dorcom
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Percentil		15th	15th Percentile:		23 MPH											
es																

29 MPH 26-35 MPH 73.7% 2491 328 9.7%

Mean Speed(Average):
10 MPH Pace Speed:
Percent in Pace:
Number of Vehicles > 35 MPH:
Percent of Vehicles > 35 MPH:

Statistics

34 MPH 37 MPH

85th Percentile : 95th Percentile :

MDM TRANSPORTATION CONSULTANTS, INC. 28 Lord Road, Suite 280 Marlborough, MA

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N/S: Salisbury Street	Street) `` }	28 Lord Ro	28 Lord Road, Suite 280	80	֭֓֞֝֟֝֟֝֟֝֟֝֟֝֟֓֓֓֓֟֟						
North of Proposed Site Driveway Holden, MA Northhound	sed Site Drive	way					Marlbor www.mdr	Marlborough, MA www.mdmtrans.com	Ē							
Start	-	16	21	26	31	36	41	46	51	56	61	99	7.1	9/		85th
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Percentii es		15th P	15th Percentile:	25	25 MPH											
		85th P 95th P	85th Percentile : 95th Percentile :	34	34 MPH 37 MPH											
Statistics	Me 16	Mean Speed(Average) 10 MPH Pace Speed	Average) :	30 MPH 26-35 MPH	30 MPH 35 MPH											
		Percent in Pace	Percent in Pace:	Σ.	76.6%											
	Number of	Number of Vehicles > 35 MPH Percent of Vehicles > 35 MPH	35 MPH:	+	360 360 10.2%											
				•	2 1											
Summary		15th P 50th P 85th P 95th P	15th Percentile: 50th Percentile: 85th Percentile: 95th Percentile:	24 29 34 37	24 MPH 29 MPH 34 MPH 37 MPH											
Statistics	Me	Mean Speed(Average) :	Average):	53	29 MPH											

☐ Crash Date

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INTERSECTION CRASH RATE WORKSHEET

CITY/TOWN : Holden, M	Α			COUNT DA	TE:	May-19
DISTRICT: 3	UNSIGN	NALIZED:	X	SIGNA	ALIZED:	
		~ IN	TERSECTION	N DATA ~		
MAJOR STREET:	Main Street	(Route 122A)			· · · · · · · · · · · · · · · · · · ·	
MINOR STREET(S):	Salisbury St	reet	······································			
INTERSECTION DIAGRAM (Label Approaches)	North N	1ain Street (3)	Salisbury (1		Main Street (4)	
		I	PEAK HOUP	R VOLUMES	F	Total Beak
APPROACH:	1	2	3	4	5	Total Peak Hourly
DIRECTION:	NB	SB	EB	WB		Approach Volume
PEAK HOURLY VOLUMES (PM) :	371		923	1,105		2,399
"K" FACTOR:	0.077	INTERS	ECTION ADT APPROACH		AL DAILY	31,156
TOTAL # OF CRASHES :	. 21	# OF YEARS :	5	CRASHES	GE#OF PERYEAR():	4.20
CRASH RATE CALCU	LATION:	0.37	RATE =	(A * 1,0 (V ·	000,000) * 365)	***************************************
Comments: MassDOT	District 3 Avg	: Signalized =	0.89; Unsign	alized = 0.61		
Project Title & Date:	1038 - Holde	n				

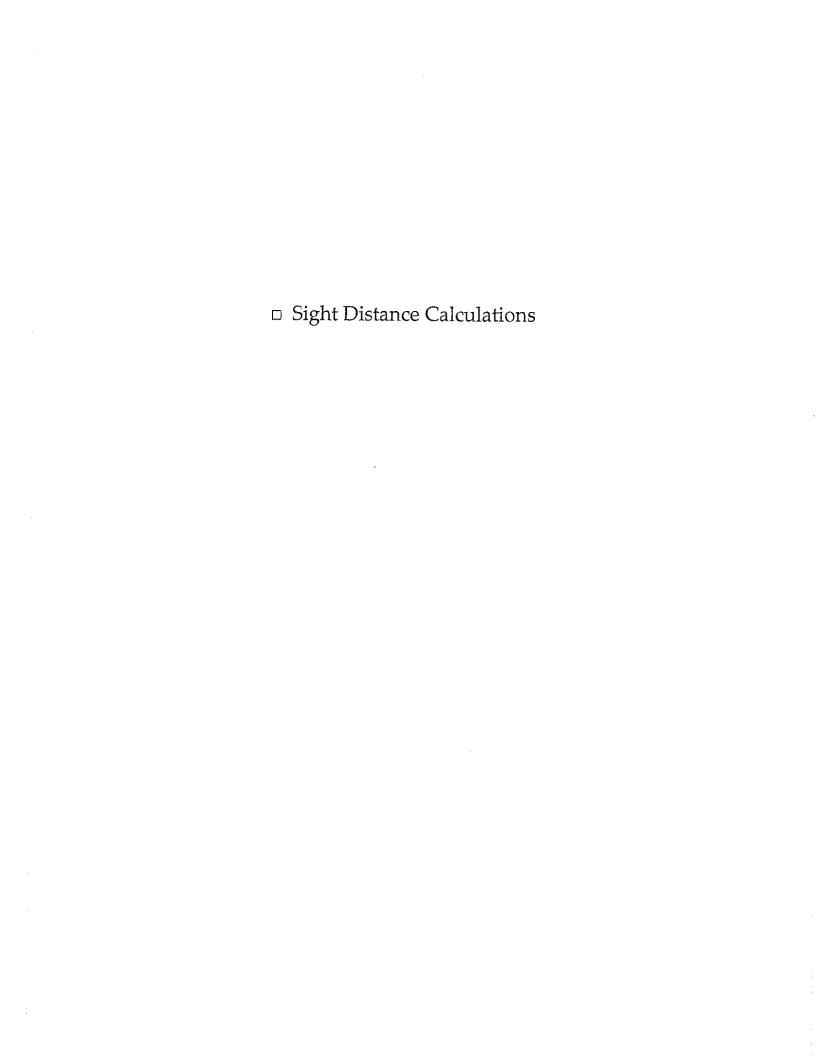


INTERSECTION CRASH RATE WORKSHEET

CITY/TOWN : Holden, M.	<u>A</u>			COUNT DA	TE:	May-19
DISTRICT: 3	UNSIGN	ALIZED :	Х	SIGNA	ALIZED:	
		~ IN1	ERSECTION	DATA ~		
MAJOR STREET :	Main Street (***************************************		
MINOR STREET(S):	Bailey Road					
	Mayo Drive					
INTERSECTION DIAGRAM (Label Approaches)	↑ North	lain Street (3)	Mayo (2 Bailey (1	t) Road	Main Street (4)	
			PEAK HOUF	VOLUMES		Total Peak
APPROACH:	1	2	3	4	5	Hourly
DIRECTION:	NB	SB	EB	WB		Approach Volume
PEAK HOURLY VOLUMES (PM) :	39	34	867	1,239		2,179
"K" FACTOR:	0.077	INTERSE	ECTION ADT APPROACH		AL DAILY	28,299
TOTAL # OF CRASHES :	12	# OF YEARS :	5	CRASHES	GE#OF PERYEAR(\):	2,40
CRASH RATE CALCU	LATION :	0.23	RATE =	(A*1,	000,000) * 365)	
Comments: MassDOT	District 3 Avg	: Signalized =	0.89; Unsign	alized = 0.6	1	
Project Title & Date:	1038 - Holde	n				

0 100sem 70,033 <u>ем</u>	rash Report for HOL	See Section 1	· · · · · · · · · · · · · · · · · · ·	にはないないというできた。	の子の大きなない	· 按 一位 第1 本公司 表 公司	United March State	A SECURITY OF	CANAL SECTION AND ASSESSMENT	である。これの日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の日本の	Carried and and the Contract of the Contract o
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Stopping Sight Distance - Regulatory

Salisbury Street approaches to Pine Street Road

		SPEED (MPH)	BRAKE REACTION DISTANCE (FT)	BRAKING DISTANCE (FT)	CALCULATED STOPPING SIGHT DISTANCE (FT)
Direction 1	NB	35	128.625	117.4	246.0
Direction 2	SB	35	128,625	117.4	246.0

<u>INPUTS</u>	Direction 1	Direction 2
Travel Direction	NB	SB
Speed	35	35
Grade	0	0
t	2.5	2.5
a	11.2	11,2

Stopping Sight Distance (SSD) - Source: AASHTO

SSD = Reaction Distance + Brake Distance

Reaction Distance = 1.47 x t x V

Brake Distance = $V^2 / (30 \times ((a/32.2)+G))$

Where:

t = reaction time (sec)

V = travel speed (mph)

G= roadway grade a - deceleration rate (ft/sec^2)

Stopping Sight Distance - 85th Percentile

Salisbury Street approaches to Pine Street Road

		SPEED (MPH)	BRAKE REACTION DISTANCE (FT)	BRAKING DISTANCE (FT)	CALCULATED STOPPING SIGHT DISTANCE (FT)
Direction 1	NB	34	124.95	110.8	235.7
Direction 2	SB	31	113.925	92.1	206.0

INPUTS	Direction 1	Direction 2
Travel Direction	NB	SB
Speed	34	31
Grade	0	0
t	2.5	2.5
а	11.2	11.2

Stopping Sight Distance (SSD) - Source: AASHTO

SSD = Reaction Distance + Brake Distance

Reaction Distance = 1.47 x t x V

Brake Distance = $V^2 / (30 \times ((a/32.2)+G))$

Where:

t = reaction time (sec)

V = travel speed (mph) G= roadway grade

a - deceleration rate (ft/sec^2)

Stopping Sight Distance - Regulatory

Bailey Road approaches to Site Driveway

		SPEED (MPH)	BRAKE REACTION DISTANCE (FT)	BRAKING DISTANCE (FT)	CALCULATED STOPPING SIGHT DISTANCE (FT)
Direction 1	NB	25	91.875	59.9	151.8
Direction 2	SB	25	91.875	59.9	151.8

INPUTS	Direction 1	Direction 2
Travel Direction	NB	SB
Speed	25	25
Grade	0	0
t	2.5	2.5
a	11.2	11.2

Stopping Sight Distance (SSD) - Source: AASHTO

SSD = Reaction Distance + Brake Distance

Reaction Distance = 1.47 x t x V

Brake Distance = $V^2 / (30 x ((a/32.2)+G))$

Where:

t = reaction time (sec)

V = travel speed (mph)
G= roadway grade
a - deceleration rate (ft/sec^2)

Stopping Sight Distance - 85th Percentile

Bailey Road approaches to Site Driveway

		SPEED (MPH)	BRAKE REACTION DISTANCE (FT)	BRAKING DISTANCE (FT)	CALCULATED STOPPING SIGHT DISTANCE (FT)
Direction 1	NB	36	132.3	124.2	256.5
Direction 2	SB	36	132.3	124.2	256.5

INPUTS	Direction 1	Direction 2
Travel Direction	NB	SB
Speed	3 6	36
Grade	0	0
t	2.5	2.5
а	11.2	11.2

Stopping Sight Distance (SSD) - Source: AASHTO

SSD = Reaction Distance + Brake Distance

Reaction Distance = 1.47 x t x V

Brake Distance = V^2 / (30 x ((a/32.2)+G))

t = reaction time (sec)

V = travel speed (mph)

G= roadway grade a - deceleration rate (ft/sec^2)

Intersection Sight Distance Calculations

Source: A Policy on Geometric Design of Highways and Street, 6th Edition; AASHTO; 2011.

ISD = 1.47 * V * t

V = speed t = time gap

t = 7.5 s for a passenger car for Left Turn from a Stop t = 6.5 s for a passenger car for Right Turn from a Stop

Salisbury Street

ISD = 1.47 * 40 * 7.5 = 441 ft **SAY 445 ft** (left-turn from a stop)

ISD = 1.47 * 40 * 6.5 = 382 ft **SAY 385 ft** (right-turn from a stop)

Intersection Sight Distance Calculations

Source: A Policy on Geometric Design of Highways and Street, 6th Edition; AASHTO; 2011.

ISD = 1,47 * V * t

V = speed t = time gap

t = 7.5 s for a passenger car for Left Turn from a Stop t = 6.5 s for a passenger car for Right Turn from a Stop

Bailey Road

ISD = 1.47 * 25 * 7.5 = 276 ft **SAY 280 ft** (left-turn from a stop)

ISD = 1.47 * 25 * 6.5 = 239 ft **SAY 240 ft** (right-turn from a stop)

□ Trip Generation Calculations	

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Institute of Transportation Engineers (ITE) 10th Edition Land Use Code (LUC) 210 - Single-Family Detached Housing

Average Vehicle Trips Ends vs:

Dwelling Units

Independent Variable (X):

AVERAGE WEEKDAY DAILY

 $T = 9.5^* (X)$

T = 9.5*12

T = 114.00

T = 114vehicle trips

with 50% (57 vpd) entering and 50% (57 vpd) exiting.

WEEKDAY MORNING PEAK HOUR OF ADJACENT STREET TRAFFIC

T = 0.74*(X)

T=0.74 *12

T = 8.88

T = 9vehicle trips

with 25% (2 vph) entering and 75% (7 vph) exiting.

WEEKDAY EVENING PEAK HOUR OF ADJACENT STREET TRAFFIC

T = 0.99*(X)

T = 0.99*12

T = 11.88

T = 12vehicle trips

with 63% (8 vph) entering and 37% (4 vph) exiting.

SATURDAY DAILY

T = 9.54*(X)

T = 9.54*12

T = 114.48

T = 114vehicle trips

with 50% (57 vph) entering and 50% (57 vph) exiting.

SATURDAY MIDDAY PEAK HOUR OF GENERATOR

T = 0.93*(X)

T = 0.93*12

T = 11.16

T = 11vehicle trips

with 54% (6 vph) entering and 46% (5 vph) exiting.

Institute of Transportation Engineers (ITE) 10th Edition Land Use Code (LUC) 220 - Multifamily Housing (Low-Rise)

Average Vehicle Trips Ends vs:

Dwelling Units

Independent Variable (X):

AVERAGE WEEKDAY DAILY

T = 7.56 (X) - 40.86

T = 7.56*90 - (40.86)

T = 639.54

T = 640vehicle trips

with 50% (320 vpd) entering and 50% (320 vpd) exiting.

WEEKDAY MORNING PEAK HOUR OF ADJACENT STREET TRAFFIC

Ln T = 0.95 Ln (X) - 0.51

Ln T = 0.95 Ln 90 - (0.51)

Ln T = 3.76

T = 43.16

T = 43vehicle trips

with 23% (10 vph) entering and 77% (33 vph) exiting.

WEEKDAY EVENING PEAK HOUR OF ADJACENT STREET TRAFFIC

Ln T = 0.89 Ln (X) - 0.02

Ln T = 0.89 Ln 90 - (0.02)

Ln T = 3.98

T = 53.78

T = 54

vehicle trips

with 63% (34 vph) entering and 37% (20 vph) exiting.

SATURDAY DAILY

T = 14.01 * (X) - 521.69

T = 14.01 *90 - (521.69)

T = 739.21

T = 740vehicle trips

with 50% (370 vpd) entering and 50% (370 vpd) exiting.

SATURDAY MIDDAY PEAK HOUR OF GENERATOR

T = 1.08 * (X) - 33.24

T = 1.08 *90 - (33.24)

T = 63.96

T = 64vehicle trips

with 50% (32 vph) entering and 50% (32 vph) exiting.

 Trip Distribution Calculations 	

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Journey-to-Work Distribution

Residence	Workniace			
Town	Town	₹	% of	% of Total
Name	Name	Workers (To Framingham)	Total	Rounded
Holden town	Worcester city	3,046	35.46%	35.5%
Holden town	Holden town	1,363	15.87%	15.9%
Holden town	Shrewsbury town	328	3.82%	3.8%
Holden town	Westborough town	312	3.63%	3.6%
Holden town	Framingham town	273	3,18%	3.2%
Holden town	Marlborough city	223	2.60%	2.6%
Holden town	West Baylston town	208	2.42%	2.4%
Holden town	Boston city	165	1.92%	1.9%
Holden town	Sterling town	131	1.52%	1.5%
Holden town	Aubum town	122	1.42%	1.4%
Holden fown	Milford town	96	1.12%	1.1%
Holden town	Leominster city	87	1.01%	1.0%
Holden town	Southborough town	85	0.99%	1.0%
Holden town	Waltham city	72	0.84%	0.8%
Holden town	Hopkîntan town	69	0.80%	%8.0
Holden town	Bedford town	53	0.78%	0.8%
Holden town	Chelmsford town	91	0.71%	0.7%
Holden town	Hudson town	59	0.69%	0.7%
Holden town	Spencer town	59	0.69%	0.7%
Holden town	Burlington town	56	0.65%	0.7%
Holden town	Acton town	55	0.64%	%9.0
Holden town	Natick town	55	0.64%	0.6%
Holden town	Oxford town	54	0.63%	0.6%
Haiden fown	Northborough town	23	0.62%	0.6%
Holden fown	Cambridge city	90	0.58%	%9'0
Holden fown	Providence cily	48	0.56%	0.6%
Holden fown	Sudbury town	46	0.54%	0.5%
Holden tawn	Graffon town	45	0.52%	0.5%
Holden town	Stoneham town	43	0.50%	0.5%
Holden town	Boylston town	42.2	0.49%	0.5%
Holden town	Millbury town	41	0.48%	0.5%
Holden town	Nashua city	39		0.5%
Other		1,138	- 1	
	Total	8,591	100.00%	100%

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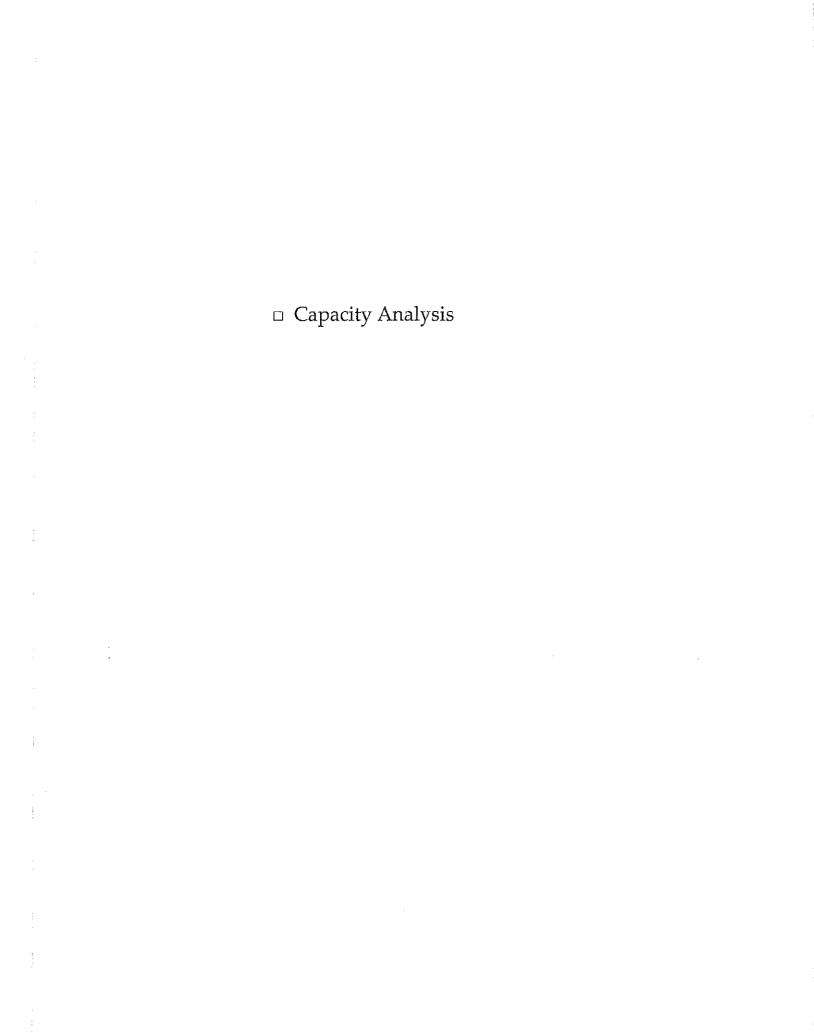
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SAY

				2	lo/From Koutes	es			
	Main Street	treet	Main Street	treet	Bailey	Bailey Road	Sailisbu	Sailisbury Street	Total
Recidence	(From East)	East)	(From West)	Vest)	(From	South)	Hor-)	(From South)	
Worcester city		%0'0		0.0%		0.0%	100%	35,5%	35.5%
Holden town	10%	1.6%	20%	7.9%	30%	4.8%	20%	3.2%	17.5%
Shrewsbury town	100%	3.8%		%0.0		%0.0		%0.0	3.8%
Westborough town	100%	3.6%		%0.0		%0.0		%0.0	3.6%
Framingham lown	100%	3.2%		0.0%		%0.0	-	%0.0	3.2%
Mariborough city	100%	2.6%		%0.0		%0'0		%0.0	2.6%
West Baylston town	100%	2.4%		0.0%		%0.0		%0.0	2.4%
Boston city	100%	1.9%		%0.0		%0'0		%0.0	1.9%
Sterling town		0.0%	100%	1.5%		%0.0		%0.0	1.5%
Aubum town	20%	0.7%		0.0%	25%	0.4%	25%	0.4%	1.4%
Milford town	100%	1.1%		0.0%		%0.0		%0.0	1.1%
Leominster city	20%	0.5%	20%	%5'0		%0.0		%0.0	1.0%
Southborough town	100%	1.0%		%0.0		0.0%		0.0%	1.0%
Waliham city	20%	0.4%	20%	0.4%		0.0%		%0.0	0.8%
Hopkinton town	100%	%8.0		%0'0		%0.0		%0'0	
Bedford town		%0.0	100%	0.8%		%0'0		%0'0	
Chelmsford town	20%	0.4%	20%	0.4%		%0'0		%0.0	0.7%
Hudson town	20%	0.3%	20%	0.3%		%0.0		0.0%	
Spencer town		%0.0	20%	0.3%	20%	0.3%	*	%0.0	0.7%
Burlington lawn	20%	0.3%	[%09	0.3%		%0°0		%0.0	0.7%
Acton town	20%	0.3%	20%	0.3%		%0.0		%0°0	0.6%
Natick town	100%	0.6%		20.0%		%0.0		0.0%	0.6%
Oxford town	%05	0.3%	_	%0.0	72%	0.2%	25%	0.2%	0.6%
Northbarough town	100%	0.6%	_	0.0%		%0.0		0.0%	0.6%
Cambridge city	20%	0.3%	20%	0.3%		%0.0		0.0%	
Providence cily	100%	%9.0		0.0%		%0.0		%0.0	
Sudbury town	100%	0.5%		%0.0		%0.0		0.0%	0.5%
Grafton town	100%	0.5%		0.0%		%0'0		%0.0	0.5%
Stoneham town	20%	0.3%	20%	0.3%		%0.0		0.0%	0.5%
Boyiston town	100%	0.5%		0.0%		%0.0		%0.0	0.5%
Milibury town	100%	0.5%	Ŧ	0.0%		%0.0		0.0%	
Nashua city		%0.0	100%	0.5%		%0.0		0.0%	0.5%
		29.7%		13.8%		2.6%		39.1%	۳
		33.7%		15.7%		6.4%		44.3%	100%

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LEVEL OF SERVICE METHODOLOGY

Capacity analysis of intersections is developed using the Synchro® computer software, which implements the methods of the 2010 Highway Capacity Manual (HCM). The resulting analysis presents a level-of-service (LOS) designation for individual intersection movements and (for signalized intersections) for the entire intersection. The LOS is a letter designation that provides a qualitative measure of operating conditions based on several factors including roadway geometry, speeds, ambient traffic volumes, traffic controls, and driver characteristics. Since the LOS of a traffic facility is a function of the traffic flows placed upon it, such a facility may operate at a wide range of LOS, depending on the time of day, day of week, or period of year. A range of six levels of service are defined on the basis of average delay, ranging from LOS A (the least delay) to LOS F (delays greater than 50 seconds for unsignalized movements, and greater than 80 seconds for signalized movements).

Signalized Intersection Performance Measures

The six LOS designations for signalized intersections may be described as follows:

- LOS A describes operations with low control delay; most vehicles do not stop at all.
- *LOS B* describes operations with relatively low control delay. However, more vehicles stop than LOS A.
- LOS C describes operations with higher control delays. Individual cycle failures may begin to appear. The number of vehicles stopping is significant at this level, although many still pass through the intersection without stopping.
- LOS D describes operations with control delay in the range where the influence of congestion becomes more noticeable. Many vehicles stop and individual cycle failures are noticeable.
- *LOS E* describes operations with high control delay values. Individual cycle failures are frequent occurrences.
- LOS F describes operations with high control delay values that often occur with over-saturation. Poor progression and long cycle lengths may also be major contributing causes to such delay levels.

The LOS for signalized intersections are calculated using the operational analysis methodology of the 2010 *Highway Capacity Manual*.¹ This method assesses the effects of signal type, timing, phasing, and progression; vehicle mix; and geometrics on delay. LOS designations are based on the criterion of control or signal delay per vehicle. Control or signal delay is a measure of driver discomfort, frustration, and fuel consumption, and includes initial deceleration delay approaching the traffic signal, queue move-up time, stopped delay and final acceleration delay. **Table A1** summarizes the relationship between LOS and control delay. The tabulated control delay criterion may be applied in assigning LOS designations to individual lane groups, to individual intersection approaches, or to entire intersections.

Table A1
LEVEL-OF-SERVICE CRITERIA
FOR SIGNALIZED INTERSECTIONS¹

	Level o	f Service
Control (Signal) Delay per Vehicle (seconds per vehicle)	v/c ≤ 1	v/c > 1
≤10.0	A	F
10.1 to 20.0	В	F
20.1 to 35.0	C	F
35.1 to 55.0	D	F
55.1 to 80.0	E	F
>80.0	F	F

¹Source: *Highway Capacity Manual 2010*, Transportation Research Board; Washington, DC; 2010.

¹Highway Capacity Manual 2010; Transportation Research Board; Washington, DC; 2010.

Unsignalized Intersection Performance Measures

The six LOS designations for unsignalized intersections may be described as follows:

- LOS A represents a condition with little or no control delay to minor street traffic.
- LOS B represents a condition with short control delays to minor street traffic.
- LOS C represents a condition with average control delays to minor street traffic.
- LOS D represents a condition with long control delays to minor street traffic.
- LOS E represents operating conditions at or near capacity level, with very long control delays to minor street traffic.
- LOS F represents a condition where minor street demand volume exceeds capacity of an approach lane, with extreme control delays resulting.

The LOS designations of unsignalized intersections are determined by application of a procedure described in the 2010 *Highway Capacity Manual*.² LOS is measured in terms of average control delay. Mathematically, control delay is a function of the capacity and degree of saturation of the lane group and/or approach under study and is a quantification of motorist delay associated with traffic control devices such as traffic signals and STOP signs. Control delay includes the effects of initial deceleration delay approaching a STOP sign, stopped delay, queue move-up time, and final acceleration delay from a stopped condition. Definitions for LOS at unsignalized intersections are also given in the *Highway Capacity Manual 2010*. **Table A2** summarizes the relationship between LOS and average control delay.

Table A2 LEVEL-OF-SERVICE CRITERIA FOR UNSIGNALIZED INTERSECTIONS¹

	Level o	f Service
Average Control Delay (seconds per vehicle)	v/c ≤ 1	v/c > 1
≤10.0	A	F
10.1 to 15.0	В	F
15.1 to 25.0	С	F
25.1 to 35.0	D	\mathbf{F}
35.1 to 50.0	E	\mathbf{F}
>50.0	F	${f F}$

¹Source: *Highway Capacity Manual 2010,* Transportation Research Board; Washington, DC; 2010.

² ibid

ntersection								
nt Delay, s/veh 0	.1		······································				<u> </u>	
Vovement	EBL	EBR	NBL	NBT	SBT	SBR		
/ol, veh/h	1	2	0	213	341	1		
Conflicting Peds, #/hr	0	0	0	0	0	0		
Sign Control	Stop	Stop	Free	Free	Free	Free		
RT Channelized	_	None	-	None	-	None		
Storage Length	0	-	-	_		-		
eh in Median Storage, #	0	_	-	0	0			
Grade, %	0	_	-	0	0	-		
Peak Hour Factor	92	92	92	92	92	92		
leavy Vehicles, %	0	0	0	2	5	0		
/vmt Flow	1	2	0	232	371	1		
Major/Minor	Minor2		Major1		Major2			
Conflicting Flow All	603	371	372	0		0		
Stage 1	371	-	-		₩	-		
Stage 2	232	_	-	-	-	-		
Critical Hdwy	6.4	6.2	4.1	-	-	-		
Critical Hdwy Stg 1	5.4	-	-	-	-	-		
Critical Hdwy Stg 2	5.4	-	•	-	-	-		
Follow-up Hdwy	3.5	3.3	2.2			-		
ot Cap-1 Maneuver	465	679	1198	-	-	-		
Stage 1	702	-	_	-	-	-		
Stage 2	811	-	_	•	-	-		
Platoon blocked, %				-	-	-		
Mov Cap-1 Maneuver	465	679	1198	-	-	-		
Mov Cap-2 Maneuver	465	-	-	-	-	-		
Stage 1	702	-		-		-		
Stage 2	811	-	-	-	•	-		
Approach	EB		NB		SB			
ICM Control Delay, s	11.1	A CONTRACTOR OF THE PARTY OF TH	0		0			
HCM LOS	В							
Minor Lane/Major Mymt	NBL	NBT EBLn1	SBT SBR					
Capacity (veh/h)	1198	- 589						
HCM Lane V/C Ratio	-	- 0.006						
HCM Control Delay (s)	0	- 11.1						
HCM Lane LOS	Å	- B						
HCM 95th %tile Q(veh)	0	- 0						

Intersection													
Int Delay, s/veh	7.7												
Movement	EBL	EBT	EBR	WBL	WBT	WBR		NBL	NBT	NBR	SBL	SBT	SBR
Vol, veh/h	12	1175	14	17	564	15		10	0	46	3	0	4
Conflicting Peds, #/hr	0	0	0	0	0	0		0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Free	Free		Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	None	-	_	None		-	-	None	· -		None
Storage Length	-	-	-	-	-	-		-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-		_	0	-	-	0	•
Grade, %	-	-2		-	3	-		-	9	-	-	-6	-
Peak Hour Factor	91	91	91	91	91	91		91	91	91	91	91	91
Heavy Vehicles, %	0	3	7	6	5	0		0	0	2	0	0	0
Mvmt Flow	13	1291	15	19	620	16		11	0	51	3	0	4
Major/Minor	Major1			Major2			M	linor1			Minor2		
Conflicting Flow All	636	0	0	1307	0	0		1993	1999	1299	2016	1998	628
Stage 1		_	-	-	-	_		1325	1325		665	665	
Stage 2	_	_	-	-	-			668	674	-	1351	1333	
Critical Hdwy	4.1	_	_	4.16	-			8.9	8,3	7.12	5,9	5,3	5.6
Critical Howy Stg 1	-	_		-	-			7.9	7.3	_	4.9	4.3	
Critical Hdwy Stg 2	-	-	-	-	-	~		7.9	7.3	-	4.9	4.3	-
Follow-up Hdwy	2.2	-	_	2,254				3.5	4	3.318	3.5	4	3.3
Pot Cap-1 Maneuver	957	_	_	517	-	-		17	22	143	86	118	540
Stage 1	-	_	-	-	-	_		100	117	_	565	575	-
Stage 2		-	-		-	_		323	326	-	294	351	-
Platoon blocked, %		-	-		-	-							
Mov Cap-1 Maneuver	957	_	_	517	-	-		16	20	143	51	106	540
Mov Cap-2 Maneuver	-		-	-	-	**		16	20	-	51	106	-
Stage 1			-	-	•			95	111	_	537	542	-
Stage 2	•	-	-		-	•		302	307	-	181	333	-
Approach	EB			WB				NB			SB		
HCM Control Delay, s	0.1			0.3				245.2			41.6		
HCM LOS				0,0			•	F			E		
Minor Lane/Major Mvmt	NBLn1	EBL	EBT	EBR WBL	WBT	WBR 8	SBLn1						
Capacity (veh/h)	59	957	-	- 517	-	_	106						
HCM Lane V/C Ratio		0.014		- 0.036	-	-	0.073						
HCM Control Delay (s)	245.2	8.8	0	- 12.2	0	-	41.6						
HCM Lane LOS	F	A	Ā	- B	Ā	_	Ē						
HCM 95th %tile Q(veh)	5	0		- 0.1	-	-	0.2						

		7	*	4	*	1
Lane Group	EBT	EBR	WBL,	WBT	NBL	NBR
Lane Configurations	4	7		414	*5	7
Volume (vph)	957	258	84	487	104	95
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
	11	11	12	12	11	11
Lane Width (ft)	-2%	• 1	12	1%	-6%	
Grade (%)	-2/6	0	0	1 70	100	0
Storage Length (ft)			0		1	1
Storage Lanes		1	25		25	1
Taper Length (ft)	4.00	4.00		0.05		1,00
Lane Util. Factor	1.00	1.00	0.95	0.95	1.00	
Frt		0.850			0.050	0.850
Flt Protected			_	0.993	0.950	1001
Satd. Flow (prot)	1801	1531	0	3347	1797	1531
Flt Permitted				0.576	0.950	
Satd. Flow (perm)	1801	1531	0	1942	1797	1531
Right Turn on Red		Yes				Yes
Satd. Flow (RTOR)		287				106
Link Speed (mph)	30			30	30	
Link Distance (ft)	600			500	800	
Travel Time (s)	13.6			11.4	18.2	
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90
	3%	3%	4%	7%	0%	5%
Heavy Vehicles (%)		287	93	541	116	106
Adj. Flow (vph)	1063	201	93	J41	110	100
Shared Lane Traffic (%)	4000	007	۸	624	116	106
Lane Group Flow (vph)	1063	287	0	634		
Enter Blocked Intersection	No	No	No	No	No	No
Lane Alignment	Left	Right	Left	Left	Left	Right
Median Width(ft)	0			0	11	
Link Offset(ft)	0			0	0	
Crosswalk Width(ft)	16			16	16	
Two way Left Turn Lane						
Headway Factor	1.03	1.03	1.01	1.01	1.01	1.01
Turning Speed (mph)		9	15		15	9
Number of Detectors	1	1	1	1	1	1
Detector Template	,	•	•	•		
Leading Detector (ft)	50	50	50	50	50	50
	0	0	0	0	0	0
Trailing Detector (ft)	0	0	0	0	0	0
Detector 1 Position(ft)		_	50	50	50	50
Detector 1 Size(ft)	50	50				
Detector 1 Type	CI+Ex	C!+Ex	CI+Ex	CI+Ex	Cl+Ex	CI+Ex
Detector 1 Channel						~ ^
Detector 1 Extend (s)	0.0	0.0	0.0	0.0	0.0	0,0
Detector 1 Queue (s)	0.0	0.0	0.0	0.0	0.0	0.0
Detector 1 Delay (s)	0.0	0.0	0.0	0.0	0.0	0.0
Turn Type	NA	Perm	pm+pt	NA	Prot	pt+ov
Protected Phases	2	•	1	6	8	81
Permitted Phases	_	2	6	_		
Detector Phase	2	2	1	6	8	8 1
	2	r.	'	•	•	
Switch Phase	40.0	10.0	6.0	10.0	6.0	
Minimum initial (s)	10.0	10.0	O.U	10.0	٠,٠	A-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1

G:\Projects\1038 - Holden (Pine Tree)\Synchro\1038 EX AM.syn MDM Transportation Consultants, Inc.

		*	*	*******		*
Lane Group	EBT	EBR	WBL	WBT	NBL.	NBR
Minimum Split (s)	15.0	15.0	11.0	15.0	11.0	
Total Split (s)	70.0	70.0	11.0	81.0	20.0	
Total Split (%)	69.3%	69.3%	10.9%	80.2%	19.8%	
Maximum Green (s)	65.0	65.0	6.0	76.0	15.0	
Yellow Time (s)	4.0	4.0	4.0	4.0	4.0	
All-Red Time (s)	1.0	1.0	1.0	1.0	1.0	
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	
Total Lost Time (s)	5.0	5.0		5.0	5.0	
Lead/Lag	Lag	Lag	Lead	0.0		
Lead-Lag Optimize?	8		2000			
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	
Recall Mode	Min	Min	None	Min	None	
Act Effct Green (s)	60.8	60.8	110,10	69.2	11.1	22.3
Actuated g/C Ratio	0.67	0.67		0.76	0.12	0.25
v/c Ratio	0,88	0.26		0.41	0.53	0.23
Control Delay	24.0	1.4		4.1	48.3	7,6
Queue Delay	0.0	0.0		0.0	0.0	0.0
Total Delay	24.0	1.4		4.1	48.3	7.6
LOS	24.0 C	Α		A	70.0 D	7.0 A
Approach Delay	19.2	~		4.1	28.9	
Approach LOS	13.2 B			4.1 A	20,5 C	
90th %ile Green (s)	65.0	65.0	6.0	76.0	15.0	
90th %ile Term Code	Max	Max	Max	Hold	Max	
70th %ile Green (s)	65.0	65.0	6.0	76.0	13.5	
70th %ile Term Code	Max	Max	Max	Hold	Gap	
50th %ile Green (s)	65.0	65.0	6.0	76.0	11.6	
. ,	Max	Max		Hold		
50th %ile Term Code 30th %ile Green (s)	53.8	53.8	Max 6.0	64.8	Gap 9.4	
30th %ile Term Code	Gap	Gap	Max	Hold	Gap	
10th %ile Green (s)	53.2	53.2	0.0	53.2	7.0	
10th %ile Term Code	Dwell	Dwell	Skip	Dwell	Gap	^
Queue Length 50th (ft)	480	0		44	69	0
Queue Length 95th (ft)	#897	27		72	125	40
Internal Link Dist (ft)	520			420	720	
Turn Bay Length (ft)	4040	4407		4704	100	440
Base Capacity (vph)	1318	1197		1701	303	442
Starvation Cap Reductn	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0
Reduced v/c Ratio	0.81	0.24		0.37	0.38	0.24
Intersection Summary						

Intersection Summary

Area Type: Other

Cycle Length: 101

Actuated Cycle Length: 90.5

Natural Cycle: 80

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.88 Intersection Signal Delay: 15.8

Intersection LOS: B

Lanes, Volumes, Timings 4: Salisbury Street & Main Street (Route 122A)

Intersection Capacity Utilization 84.5%

ICU Level of Service E

Analysis Period (min) 15
90th %ile Actuated Cycle: 101
70th %ile Actuated Cycle: 99.5
50th %ile Actuated Cycle: 97.6
30th %ile Actuated Cycle: 84.2
10th %ile Actuated Cycle: 70.2

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Int Delay, s/veh	0						
Movement	EBL	EBR	NBL	NBT	SBT	SBR	
Vol, veh/h	1	0	2	370	347	1	
Conflicting Peds, #/hr	0	0	0	0	0	0	
Sign Control	Stop	Stop	Free	Free	Free	Free	
RT Channelized	-	None	-	None	-	None	
Storage Length	0	-	-		-	•	
Veh in Median Storage, #	0	-	-	0	0	-	
Grade, %	0		-	0	0	-	
Peak Hour Factor	92	92	92	92	92	92	
Heavy Vehicles, %	0	0	0	2	5	0	
Mvmt Flow	1	0	2	402	377	1	
Major/Minor	Minor2		Major1	_,,	Major2		
Conflicting Flow All	785	378	378	0	•	0	
Stage 1	378	-	-	-		-	
Stage 2	407		-	-	-	-	
Critical Hdwy	6.4	6.2	4.1	-	-	•	
Critical Hdwy Stg 1	5,4	-	-	-	-	-	
Critical Hdwy Stg 2	5,4		-	_	-		
Follow-up Hdwy	3,5	3,3	2.2	_	-	٠	
Pot Cap-1 Maneuver	364	673	1192	-		-	
Stage 1	697	-	-	-	-	-	
Stage 2	676		-	-	-	-	
Platoon blocked, %				-	-		
Mov Cap-1 Maneuver	363	673	1192	_	-	-	
Mov Cap-2 Maneuver	363	_	-	_	-	-	
Stage 1	697		-	_		_	
Stage 2	675	-	-	-	-	-	
			1.Im				
Approach	EB		NB -	····	SB		
ICM Control Delay, s	14.9		0		0		
HCM LOS	В						
Minor Lane/Major Mymt	NBL	NBT EBLn1	SBT SBR				
Capacity (veh/h)	1192	- 363			······································		V - 11 k
ICM Lane V/C Ratio	0.002	- 0.003					
ICM Control Delay (s)	8	0 14.9					
HCM Lane LOS	A	A B					
HCM 95th %tile Q(veh)	0	- 0					

Intersection												······································
Int Delay, s/veh	7.6				-							
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	. NBT	NBR	SBL	SBT	SBR
Vol. veh/h	12	828	27	33	1191	15	8	1	30	12	0	22
Conflicting Peds, #/hr	0	0	0	0	0	0	(0	0	0	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	None	-	-	None			None	-	-	None
Storage Length	-	-	-		-	-			-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-		•	-	-	0	-
Grade, %		-2	-		3	-		- 9	-	-	-6	
Peak Hour Factor	97	97	97	97	97	97	97	97	97	97	97	97
Heavy Vehicles, %	0	1	0	3	1	7	() 0	7	8	0	0
Mvmt Flow	12	854	28	34	1228	15	8	3 1	31	12	0	23
Major/Minor	. Major1			Мајог2			Minor			Minor2		
Conflicting Flow All	1243	0	0	881	0	0	220		868	2212	2210	1236
Stage 1	1240	· ·	-	-	_	~	892		-	1304	1304	-
Stage 2	_	_	_	-		-	131		_	908	906	_
Critical Hdwy	4.1	_	-	4.13	_	**	8.9		7.17	5.98	5.3	5.6
Critical Hdwy Stg 1	-7. i	_	_	7.10	_		7.9		-	4.98	4.3	_
Critical Hdwy Stg 2	_	_	_		_	_	7.9		_	4.98	4.3	-
Follow-up Hdwy	2.2	_		2.227	_	-	3.8		3.363	3.572	4	3.3
Pot Cap-1 Maneuver	567	_	_	763	_	-	1:			63	93	267
Stage 1	-	_	_	700		_	21			296	359	
Stage 2	_	_	_	_			102			435	484	
Platoon blocked, %	_	_			_	_	. •				, - ,	
Mov Cap-1 Maneuver	567	_	_	763		_	(12	277	45	76	267
Mov Cap-1 Maneuver	201		_	700	_	_	,			45	76	
	•	-	_	_	_	_	20			284	307	_
Stage 1 Stage 2	-	-	-	-	-		80			368	464	
										0.0		
Approach	EB			WB			NE 1 To a			SB		
HCM Control Delay, s HCM LOS	0.2			0.3			\$ 351 1			61.8 F		
Minor Lane/Major Mvmt	NBLn1	EBL	EBT	EBR WBL	WBT	WBR S						
Capacity (veh/h)	36	567		- 763	-	-	97					
HCM Lane V/C Ratio	1.117			- 0.045	-		0.361					
HCM Control Delay (s)	\$ 357	11.5	0	- 9.9	0	-	61.8					
HCM Lane LOS	F	В	Ā	- A	Α	-	F					
HCM 95th %tile Q(veh)	4.2	0.1	-	- 0.1	-	-	1.4					
Notes		_, · · · · · · · · · · · · · · · · · · ·		20 May 1 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1								Martin State
~: Volume exceeds capac	city \$: De	elay exc	ceeds 30	00s +: Com	putatio	n Not De	efined *: A	II major	volume i	in platoon		

		*	*	4	*	*
Lane Group	CDT	במח	/WD1 -	\AIDT	NIDI	
Lane Group	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations	_ ^	7		41	¥	7
Volume (vph)	717	206		963	250	121
ldeal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Lane Width (ft)	11	11	12	12	11	11
Grade (%)	-2%			1%	-6%	
Storage Length (ft)		0	0		100	0
Storage Lanes		1	Ō		1	1
Taper Length (ft)		•	25		25	
Lane Util, Factor	1.00	1.00		0.95	1.00	1.00
Frt	1.00		0.50	0.90	1.00	
		0.850		0.004		0.850
Flt Protected			_	0.994	0.950	
Satd. Flow (prot)	1837	1561	0	3535	1779	1592
Fit Permitted				0.588	0,950	
Satd. Flow (perm)	1837	1561	0	2091	1779	1592
Right Turn on Red		Yes				Yes
Satd. Flow (RTOR)		212				125
Link Speed (mph)	30	416		30	30	120
Link Distance (ft)	600					
				500	800	
Travel Time (s)	13.6			11.4	18.2	
Peak Hour Factor	0.97	0.97	0.97	0.97	0.97	0,97
Heavy Vehicles (%)	1%	1%	1%	1%	1%	1%
Adj. Flow (vph)	739	212	146	993	258	125
Shared Lane Traffic (%)						
Lane Group Flow (vph)	739	212	0	1139	258	125
Enter Blocked Intersection	No	No	No	No	No	No
Lane Alignment	Left	Right	Left	Left	Left	Right
Median Width(ft)	0	Main	Ľ.	0	11	Ngut
Link Offset(ft)	0			0	0	
Crosswalk Width(ft)	16			16	16	
Two way Left Turn Lane						
Headway Factor	1.03	1.03	1.01	1.01	1.01	1.01
Turning Speed (mph)		9	15		15	9
Number of Detectors	1	1	1	1	1	1
Detector Template	•	•	•	•	•	•
Leading Detector (ft)	50	50	50	50	50	50
Trailing Detector (ft)	0	0	0	0		
Detector 1 Position(ft)					0	0
	0	0	0	0	0	0
Detector 1 Size(ft)	50	50	50	50	50	50
Detector 1 Type	CI+Ex	CI+Ex	CI+Ex	CI+Ex	CI+Ex	CI+Ex
Detector 1 Channel						
Detector 1 Extend (s)	0.0	0.0	0.0	0.0	0.0	0.0
Detector 1 Queue (s)	0.0	0.0	0.0	0.0	0.0	0.0
Detector 1 Delay (s)	0.0	0.0	0.0	0.0	0.0	0.0
Turn Type	NA	Perm	pm+pt	NA	Prot	
Protected Phases		1 63111	₩			pt+ov
	2	^	1	6	8	8 1
Permitted Phases	_	2	6	_	_	
Detector Phase	2	2	1	6	8	8 1
Switch Phase						
Minimum Initial (s)	10.0	10.0	6.0	10.0	6.0	

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		*	✓	4	*	*
Lane Group	EBT	EBR	WBL.	WBT	NBL	NBR
Minimum Split (s)	15.0	15.0	11.0	15.0	11.0	
Total Split (s)	45.0	45.0	11.0	56,0	17.0	
Total Split (%)	61.6%	61.6%	15.1%	76.7%	23.3%	
Maximum Green (s)	40.0	40.0	6.0	51.0	12.0	
Yellow Time (s)	4.0	4.0	4.0	4.0	4.0	
All-Red Time (s)	1.0	1.0	1.0	1.0	1.0	
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	
Total Lost Time (s)	5.0	5.0		5.0	5.0	
Lead/Lag	Lag	Lag	Lead			
Lead-Lag Optimize?	5	3				
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	
Recall Mode	Min	Min	None	Min	None	
Act Effct Green (s)	31.9	31.9		40.2	11.9	23.2
Actuated g/C Ratio	0.51	0.51		0.64	0.19	0.37
v/c Ratio	0.79	0.24		0.78	0.76	0.19
Control Delay	20.3	2.1		10.9	44.8	4.9
Queue Delay	0.0	0.0		0.0	0,0	0.0
Total Delay	20.3	2.1		10.9	44.8	4.9
LOS	20.0 C	Α		В	D	A
Approach Delay	16.2			10.9	31.8	
Approach LOS	В			В	C	
90th %ile Green (s)	40.0	40.0	6.0	51.0	12.0	
90th %ile Term Code	⊸o.o Max	Max	Max	Max	Max	
70th %ile Green (s)	38.3	38.3	6.0	49.3	12.0	
70th %ile Term Code	Gap	Gap	Max	Hold	Max	
50th %ile Green (s)	31.3	31.3	6,0	42.3	12.0	
50th %ile Term Code	Gap	Gap	Max	Hold	Max	
30th %ile Green (s)	25.4	25.4	6.0	36.4	12.0	
30th %ile Term Code	Gap	Gap	Max	Hold	Max	
10th %ile Green (s)	25.0	25.0	0.0	25.0	10.2	
10th %ile Term Code	Dwell	Dwell	Skip	Dwell	Gap	
Queue Length 50th (ft)	232	0	2.00	98	97	0
Queue Length 95th (ft)	368	27		132	#243	34
Internal Link Dist (ft)	520	 ,		420	720	•
Turn Bay Length (ft)	OLU				100	
Base Capacity (vph)	1212	1102		1811	352	649
Starvation Cap Reductn	0	0		0	0	0.0
Spillback Cap Reductn	0	0		0	Ö	Ŏ
Storage Cap Reductn	0	0		0	0	Ő
Reduced v/c Ratio	0.61	0.19		0.63	0.73	0.19
	0.01	0.10		0,00	0.,0	0.10
Intersection Summary						

Area Type:

Other

Cycle Length: 73

Actuated Cycle Length: 62.4

Natural Cycle: 60

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.79
Intersection Signal Delay: 16.2

Intersection LOS: B

Lanes, Volumes, Timings

4: Salisbury Street & Main Street (Route 122A)

2019 Baseline Conditions Weekday Evening Peak Hour

Intersection Capacity Utilization 94.8%

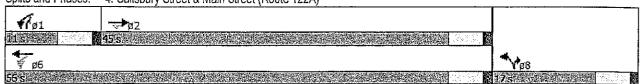
ICU Level of Service F

Analysis Period (min) 15
90th %ile Actuated Cycle: 73
70th %ile Actuated Cycle: 71.3
50th %ile Actuated Cycle: 64.3
30th %ile Actuated Cycle: 58.4
10th %ile Actuated Cycle: 45.2

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Splits and Phases: 4: Salisbury Street & Main Street (Route 122A)



Intersection							
	.1						
Movement	EBL	EBR	NBL	NBT	SBT	SBR	
Vol, veh/h	1	2	0	203	350	1	
Conflicting Peds, #/hr	0	0	0	0	0	0	
Sign Control	Stop	Stop	Free	Free	Free	Free	
RT Channelized	·-	None	-	None		None	
Storage Length	0	-	-	-			
Veh in Median Storage, #	0	-	-	0	0	-	
Grade, %	0	-	-	0	0	-	
Peak Hour Factor	92	92	92	92	92	92	
Heavy Vehicles, %	0	0	0	2	5	0	
Mvmt Flow	1	2	0	221	380	1	
Major/Minor	Minor2		Major1		Major2		
Conflicting Flow All	602	381	382	0	-	0	
Stage 1	381	-	-	-	-	-	
Stage 2	221	-	-	-	-	-	
Critical Hdwy	6.4	6,2	4.1	-		-	
Critical Hdwy Stg 1	5.4	-	-	-	-	-	
Critical Hdwy Stg 2	5.4	-	-	-	-	-	
Follow-up Hdwy	3.5	3.3	2.2	-	-	-	
Pot Cap-1 Maneuver	466	671	1188	•	-	-	
Stage 1	695		-	-	-	•	
Stage 2	821	-		-	-	-	
Platoon blocked, %				-	•	-	
Mov Cap-1 Maneuver	466	671	1188	-	-	-	
Mov Cap-2 Maneuver	466	-	_	-	-	-	
Stage 1	695	_			-	-	
Stage 2	821	-		-	-	-	
Approach	EB		ΝB		SB		
HCM Control Delay, s	11.2		0		0		
HCM LOS	В		v		_		
Minor Lane/Major Mvmt	NBL	NBT EBLn1	SBT SBR				
Capacity (veh/h)	1188	- 585					
HCM Lane V/C Ratio	- 100	- 0.006					
HCM Control Delay (s)	0	- 11.2					
HCM Lane LOS	Ā	- B					
HCM 95th %tile Q(veh)	0	- 0					

Intersection														
Int Delay, s/veh	9.2			·									******	
Movement	mo!	еот	EDO	1.6	וחו	WOT	WDD		NIDI	NOT	UDD	o ni	A	0.00
· · · · · · · · · · · · · · · · · · ·	EBL		EBR		/BL	WBT	WBR		NBL	NBT	NBR	SBL	SBT	SBR
Vol, veh/h	12		14		17	578	15		10	0	47	3	0	4
Conflicting Peds, #/hr	0		0	- -	0	0	0		0	0	0	0	0	0
Sign Control	Free		Free	F	ree	Free	Free		Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	None		-	-	None		-	•	None	-	•	None
Storage Length	-	_	•		-	-	-		-	-	-	-	-	-
Veh in Median Storage, #		0	-		-	0	-		-	0	-	-	0	-
Grade, %	-	_	-		-	3			-	9	-	-	-6	-
Peak Hour Factor	91		91		91	91	91		91	91	91	91	91	91
Heavy Vehicles, %	0	_	7		6	5	0		0	0	2	0	0	0
Mvmt Flow	13	1324	15		19	635	16		11	0	52	3	0	4
Major/Minor	Major1			Majo	or2				Minor1			Minor2		
Conflicting Flow All	652	0	0		340	0	0		2041	2047	1332	2065	2047	643
Stage 1	002	-	-	10		-	-		1358	1358	1002	681	681	040
Stage 2		_	_		_	_	_		683	689	_	1384	1366	-
Critical Hdwy	4.1	_	_	A	.16	_	_		8.9	8.3	7.12	5.9	5.3	5.6
Critical Hdwy Stg 1		_	_	7,	. 10	_	_		7.9	7.3	1.12	4.9	4.3	0.0
Critical Hdwy Stg 2	_	_	-			_	_		7.9	7.3	_	4.9	4.3	-
Follow-up Hdwy	2.2	_	_	2.2	54	_			3.5	4	3.318	3.5	4.5	3.3
Pot Cap-1 Maneuver	944	_	_		02	_	_		15	20	135	81	112	531
Stage 1	0.1	_	_	U	-		_		94	111	,00	557	569	551
Stage 2	_	_	_		_	_	_		314	319		284	342	•
Platoon blocked, %			-		-	_	_		3 (4	010	-	204	J42	-
Mov Cap-1 Maneuver	944	_		5	02	_	_		14	18	135	46	100	531
Mov Cap-2 Maneuver	V77 _	_	_	J	-	_	_		14	18	100	46	100	991
Stage 1	_	_	_		_	_	-		89	105	-	527	535	-
Stage 2	-	-	-			-	-		293	300	-	166	324	_
Approach	EB				VB_				NB			SB		
HCM Control Delay, s	0.1			0	0,3				297.6			45.7		
HCM LOS									F			Е		
Minor Lane/Major Mvmt	NBLn1	EBL	EBT	EBR W	₽I	WBT	WBR S	RI n1						
Capacity (veh/h)	54	944	LDI		02	VYD1	MORG	96					·	
HCM Lane V/C Ratio		0.014	-	- 0.03		-	-	0.08						
HCM Control Delay (s)	297.6	8.9	- 0		37 2.4	0	-							
HCM Lane LOS	297.0 F		0 A	- 12	2.4 B	0	-	45.7						
HCM 95th %tile Q(veh)	5.4	A	A -),1	A -	-	E						
LICHAL SOUL WING M(AGIL)	0.4	0	-	- 0	7, 1	-	-	0.3						

4: Salisbury Street & Main Street (Route 122A)

			~	······································		
		*	•	4	*	/
Lane Group	EBT	EBR	WBL	WBT	NBL	NBR
		74	VVDL			*
Lane Configurations	†	•	00	414) 107	
Volume (vph)	981	265	86	499	107	97
Ideal Flow (vphpi)	1900	1900	1900	1900	1900	1900
Lane Width (ft)	11	11	12	12	11	11
Grade (%)	-2%			1%	-6%	
Storage Length (ft)		0	0		100	0
Storage Lanes		1	0		1	1
Taper Length (ft)			25		25	
Lane Util. Factor	1.00	1.00	0.95	0.95	1.00	1.00
Frt		0.850	*			0.850
Flt Protected		0.000		0,993	0.950	0.000
Satd. Flow (prot)	1801	1531	0	3347	1797	1531
	1001	1001	U	0.562	0.950	1001
Fit Permitted	4004	4504	^			4504
Satd. Flow (perm)	1801	1531	0	1894	1797	1531
Right Turn on Red		Yes				Yes
Satd. Flow (RTOR)		294				108
Link Speed (mph)	30			30	30	
Link Distance (ft)	600			500	800	
Travel Time (s)	13,6			11.4	18.2	
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90
Heavy Vehicles (%)	3%	3%	4%	7%	0,00	5%
		294	96	554	119	108
Adj. Flow (vph)	1090	294	90	004	119	100
Shared Lane Traffic (%)	1000	667	<i>n</i>	000		400
Lane Group Flow (vph)	1090	294	.0	650	119	108
Enter Blocked Intersection	No	No	No	No	No	No
Lane Alignment	Left	Rìght	Left	Left	Left	Right
Median Width(ft)	0	-		0	11	
Link Offset(ft)	0			0	0	
Crosswalk Width(ft)	16			16	16	
Two way Left Turn Lane				, ,		
Headway Factor	1,03	1.03	1.01	1.01	1.01	1 .01
	1,03			1.01	1.01	
Turning Speed (mph)		9	15			9
Number of Detectors	1	1	1	1	1	1
Detector Template	_ •					
Leading Detector (ft)	50	50	50	50	50	50
Trailing Detector (ft)	0	0	0	0	0	0
Detector 1 Position(ft)	0	0	0	0	0	0
Detector 1 Size(ft)	50	50	50	50	50	50
Detector 1 Type	CI+Ex	Cl+Ex	CI+Ex	CI+Ex	CI+Ex	CI+Ex
Detector 1 Channel	71 HA	-1: -1	-: -		n	/-
Detector 1 Extend (s)	0.0	0.0	0.0	0.0	0.0	0.0
						0.0
Detector 1 Queue (s)	0.0	0.0	0.0	0.0	0.0	
Detector 1 Delay (s)	0.0	0.0	0.0	0.0	0.0	0.0
Turn Type	NA	Perm	pm+pt	NA	Prot	pt+ov
Protected Phases	2		1	6	8	8 1
Permitted Phases		2	6			
Detector Phase	2	2	1	6	8	8 1
Switch Phase						
Minimum Initial (s)	10.0	10.0	6.0	10.0	6.0	
ivariatium muar (a)	10.0	10.0	0.0	10.0	0.0	

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		~	•	***	*	1	
Lane Group	EBT	EBR	WBL	WBT	NBL	NBR	
Minimum Split (s)	15.0	15.0	11.0	15.0	11.0		
Total Split (s)	70.0	70.0	11.0	81.0	20.0		
Total Split (%)	69.3%	69.3%	10.9%	80.2%	19.8%		
Maximum Green (s)	65.0	65.0	6.0	76.0	15.0		
Yellow Time (s)	4.0	4.0	4.0	4.0	4.0		
All-Red Time (s)	1.0	1.0	1.0	1.0	1.0		
Lost Time Adjust (s)	0.0	0.0		0.0	0.0		
Total Lost Time (s)	5.0	5.0		5.0	5.0		
Lead/Lag	Lag	Lag	Lead				
Lead-Lag Optimize?							
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0		
Recall Mode	Min	Min	None	Min	None		
Act Effct Green (s)	62.6	62.6		71.1	11.3	22.5	
Actuated g/C Ratio	0.68	0.68		0.77	0.12	0.24	
v/c Ratio	0.89	0.26		0.43	0.54	0.24	
Control Delay	25.5	1.4		4.2	49.3	7.5	
Queue Delay	0.0	0.0		0.0	0.0	0.0	
Total Delay	25.5	1.4		4.2	49.3	7.5	
LOS	С	Α		Α	D	Α	
Approach Delay	20.4			4.2	29.4		
Approach LOS	С			Α	С		
90th %ile Green (s)	65.0	65.0	6.0	76.0	15.0		
90th %ile Term Code	Max	Max	Max	Hold	Max		
70th %ile Green (s)	65.0	65.0	6.0	76.0	13.7		
70th %ile Term Code	Max	Max	Max	Hold	Gap		
50th %ile Green (s)	65.0	65.0	6.0	76.0	11.7		
50th %ile Term Code	Max	Max	Max	Hold	Gap		
30th %ile Green (s)	59.1	59.1	6.0	70.1	9.8		
30th %ile Term Code	Gap	Gap	Max	Hold	Gap		
10th %ile Green (s)	57.0	57.0	0.0	57.0	7.2		
10th %ile Term Code	Dwell	Dwell	Skip	Dwell	Gap		
Queue Length 50th (ft)	513	0		46	71	0	
Queue Length 95th (ft)	#935	28		74	127	41	
Internal Link Dist (ft)	520			420	720		
Turn Bay Length (ft)					100		
Base Capacity (vph)	1282	1174		1639	295	438	
Starvation Cap Reductn	0	0		0	0	0	
Spillback Cap Reductn	0	0		0	0	0	
Storage Cap Reductn	0	0		0	0	0	
Reduced v/c Ratio	0.85	0.25		0.40	0.40	0.25	
Intersection Summary							

MICESCONON OUTIN

Area Type: Other

Cycle Length: 101

Actuated Cycle Length: 92.5

Natural Cycle: 80

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.89 Intersection Signal Delay: 16.7

Intersection LOS: B

2024 No-Build Conditions Weekday Morning Peak Hour

4: Salisbury Street & Main Street (Route 122A)

Intersection Capacity Utilization 86.4%

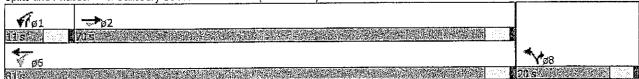
ICU Level of Service E

Analysis Period (min) 15
90th %ile Actuated Cycle: 101
70th %ile Actuated Cycle: 99.7
50th %ile Actuated Cycle: 97.7
30th %ile Actuated Cycle: 89.9
10th %ile Actuated Cycle: 74.2

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Splits and Phases: 4: Salisbury Street & Main Street (Route 122A)



Intersection								
Int Delay, s/veh	0			· · · · ·		, , , , , , , , , , , , , , , , , , ,		
Movement	EBL	EBR	ı	NBL	NBT	SBT	SBR	
Vol, veh/h	1	0		2	379	356	1	
Conflicting Peds, #/hr	0	0		0	0	0	0	
Sign Control	Stop	Stop	F	ree	Free	Free	Free	
RT Channelized	· -	None		-	None	-	None	
Storage Length	0	No.			-	-	-	
Veh in Median Storage, #	0	-		-	0	0	-	
Grade, %	0	-		-	0	0		
Peak Hour Factor	92	92		92	92	92	92	
Heavy Vehicles, %	0	0		0	2	5	0	
Mvmt Flow	1	0		2	412	387	1	
Major/Minor	Minor2			jor1		Major2		
Conflicting Flow All	804	388	;	388	0	-	0	
Stage 1	388	-		•	-	-	-	
Stage 2	416	-		-	-	-	-	
Critical Hdwy	6.4	6.2		4.1	-	-		
Critical Howy Stg 1	5.4	-		-	-	-	-	
Critical Hdwy Stg 2	5.4	-		-	-	-	-	
Follow-up Hdwy	3.5	3.3		2.2	-	•	-	
Pot Cap-1 Maneuver	355	665	1	182	-		-	
Stage 1	690	-		-	-		-	
Stage 2	670	-		~		-	-	
Platoon blocked, %						-	-	
Mov Cap-1 Maneuver	354	665	1.	182	-	_	-	
Mov Cap-2 Maneuver	354	-		-	-		-	
Stage 1	690	-		-	-	-	-	
Stage 2	669	-		-	-	-	-	
Annroach	ED			A ATTO		0.0		
Approach	EB			NB		SB		
HCM Control Delay, s HCM LOS	15.2			0		0		
HUIVI LUS	С							
Minor Lane/Major Mvmt	NBL	NBT EBLn1	SBT S	BR				
Capacity (veh/h)	1182	- 354						
HCM Lane V/C Ratio	0.002	- 0.003	_	_				
HCM Control Delay (s)	8.1	0 15,2	_					
HCM Lane LOS	A	A C	-	_				
HCM 95th %tile Q(veh)	Ô	- 0	_	_				

Intersection									·····		·····	
Int Delay, s/veh	10.6											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBI	NBT	NBR	SBL	SBT	SBR
Vol, veh/h	12	849	28	34	1221	15		3 1	31	12	0	23
Conflicting Peds, #/hr	0	0	0	0	0	0	(0	0	0	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Stop	Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	None	-	-	None			None	-	-	None
Storage Length	-	_	-	-	-	-			-	-	-	
Veh in Median Storage, #	-	0	_	-	0	-		- 0	-	-	0	-
Grade, %	-	-2	-	-	3	-		. 9	-	-	-6	
Peak Hour Factor	97	97	97	97	97	97	9	97	97	97	97	97
Heavy Vehicles, %	0	1	0	3	1	7	(0 (7	8	0	0
Mymt Flow	12	875	29	35	1259	15		3 1	32	12	0	24
Major/Minor	Major1			Major2			Minor			Minor2		
Conflicting Flow All	1274	0	0	904	0	0	226	2258	890	2268	2266	1266
Stage 1	-	-	-	•	-	-	914	914	_	1337	1337	-
Stage 2	-	-	-	-	-	-	1348	1344	-	931	929	-
Critical Hdwy	4.1	-	-	4.13	_	-	8.9	8.3	7.17	5.98	5,3	5,6
Critical Hdwy Stg 1	-	_	-	-	_	-	7.9	7.3	-	4.98	4.3	-
Critical Hdwy Stg 2	-	_	-	_		-	7.9	7.3	-	4.98	4.3	-
Follow-up Hdwy	2.2	_		2.227	_	-	3.5	5 4	3.363	3.572	4	3.3
Pot Cap-1 Maneuver	552	-	-	748	_	_	(3 13	268	59	88	257
Stage 1	-	-	_	-	_	-	209	225		286	350	_
Stage 2		_	-	_	-	_	9(-	426	476	_
Platoon blocked, %		_	-		_	_	-					
Mov Cap-1 Maneuver	552	_	_	748	_	_	~ *	' 10	268	41	71	257
Mov Cap-2 Maneuver		_			_	_	~			41	71	
Stage 1	_		_		_	_	200		_	273	294	_
Stage 2	-	-	-	-	_	-	7:		-	357	455	-
Approach	EB			WB			NE			SB		
HCM Control Delay, s	0.2			0.3			\$ 521.	5		67.4		
HCM LOS							F	;		F		
Minor Lang/Major Mumi	NBLn1	EBL	בסד	EBR WBL	WBT	WBR 9	2DI n1					
Minor Lane/Major Mymt			EBT		YYDI	YYOR			····			
Capacity (veh/h)	29	552	-	- 748	-	-	92					
HCM Cantral Dalay (a)		0.022		- 0.047	~		0.392					
HCM Control Delay (s)	\$ 521.5	11.7	0	- 10	0	-	67.4					
HCM Lane LOS	F	В	Α	- B	Α	-	F					
HCM 95th %tile Q(veh)	4.8	0.1	-	- 0.1	-	-	1.6					
Notes												
~: Volume exceeds capac	ity \$: De	elay exc	eeds 30	00s +: Com	putation	n Not De	fined *: A	ll major v	volume i	n platoon		

	·	1	Le	4	*	<i>></i>
1 0		7	₹		ì	- /
Lane Group	EBT	EBR		WBT	NBL	NBR
Lane Configurations	↑	*		414	**	*
Volume (vph)	735	211	146	987	256	124
ldeal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Lane Width (ft)	11	11	12	12	11	11
Grade (%)	-2%			1%	-6%	
Storage Length (ft)		0	0	1,0	100	0
Storage Lanes		1	ŏ		1	1
Taper Length (ft)			25		25	1
Lane Util. Factor	1.00	1.00		0.95	1.00	1.00
Frt	1.00			0.80	1.00	
Flt Protected		0.850		0.004	0.050	0.850
	4007	4504	_	0,994	0.950	
Satd. Flow (prot)	1837	1561	0	3535	1779	1592
Flt Permitted				0.575	0.950	
Satd. Flow (perm)	1837	1561	0	2045	1779	1592
Right Turn on Red		Yes				Yes
Satd. Flow (RTOR)		218				128
Link Speed (mph)	30			30	30	
Link Distance (ft)	600			500	800	
Travel Time (s)	13.6			11.4	18.2	
Peak Hour Factor	0.97	0.97	0.97	0.97	0.97	0.97
Heavy Vehicles (%)	1%	1%	1%	1%	1%	1%
Adj. Flow (vph)	758	218	151			
Shared Lane Traffic (%)	100	210	101	1018	264	128
	750	040	•	4400		
Lane Group Flow (vph)	758	218	. 0	1169	264	128
Enter Blocked Intersection	No	No	No	No	No	No
Lane Alignment	Left	Right	Left	Left	Left	Right
Median Width(ft)	0			0	11	
Link Offset(ft)	0			0	0	
Crosswalk Width(ft)	16			16	16	
Two way Left Turn Lane						
Headway Factor	1.03	1.03	1.01	1.01	1.01	1.01
Turning Speed (mph)		9	15	, 10 1	15	9
Number of Detectors	1	1	1	1	1	1
Detector Template	J	,	,	1	ı	ı
Leading Detector (ft)	50	50	EΛ	EΩ	E0	50
• • • •		50	50	50	50	50
Trailing Detector (ft)	0	0	0	0	0	0
Detector 1 Position(ft)	0	0	0	0	0	0
Detector 1 Size(ff)	50	50	50	50	50	50
Detector 1 Type	CI+Ex	CI+Ex	CI+Ex	CI+Ex	CI+Ex	Cl+Ex
Detector 1 Channel						
Detector 1 Extend (s)	0.0	0.0	0.0	0.0	0.0	0.0
Detector 1 Queue (s)	0.0	0.0	0.0	0.0	0.0	0.0
Detector 1 Delay (s)	0.0	0.0	0.0	0.0	0.0	0.0
Turn Type	NA					
Protected Phases	2	Perm	pm+pt	NA	Prot	pt+ov
	2	^	1	6	8	8 1
Permitted Phases	_	2	6	-		
Detector Phase	2	2	1	6	8	81
Switch Phase						
Minimum Initial (s)	10.0	10.0	6.0	10.0	6.0	

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4: Salisbury Street & Main Street (Route 122A)

		*	*	*******	*	1
Lane Group	EBT	EBR	WBL	WBT	NBL	NBR
Minimum Split (s)	15.0	15.0	11.0	15.0	11.0	
Total Split (s)	45.0	45.0	11.0	56.0	17.0	
Total Split (%)	61.6%	61.6%	15.1%	76.7%	23.3%	
Maximum Green (s)	40.0	40.0	6.0	51.0	12.0	
Yellow Time (s)	4.0	4.0	4.0	4.0	4.0	
All-Red Time (s)	1.0	1.0	1.0	1.0	1.0	
Lost Time Adjust (s)	0.0	0.0	•	0.0	0.0	
Total Lost Time (s)	5.0	5.0		5.0	5.0	
Lead/Lag	Lag	Lag	Lead	0.0	0.0	
Lead-Lag Optimize?	_09	9	2000			
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	
Recall Mode	Min	Mín	None	Min	None	
Act Effet Green (s)	32.7	32,7	IVOIIC	41.0	12.0	23,3
Actuated g/C Ratio	0.52	0,52		0.65	0.19	0.37
v/c Ratio	0.80	0.24		0.82	0.78	0.19
Control Delay	20.8	2.1		12.1	46.9	4.9
	0,0	0.0		0.0	0.0	0.0
Queue Delay		2.1		12.1	46.9	4.9
Total Delay LOS	20,8 C	Z. 1 A			40.9 D	
		A		B 12.1	33,2	Α
Approach Delay	16.6				33,2 C	
Approach LOS	B	40.0	0.0	B		
90th %ile Green (s)	40.0	40.0	6.0	51.0	12.0	
90th %ile Term Code	Max	Max	Max	Max	Max	
70th %ile Green (s)	39.7	39.7	6.0	50.7	12.0	
70th %ile Term Code	Gap	Gap	Max	Hold	Max	
50th %ile Green (s)	32.4	32,4	6.0	43.4	12.0	
50th %ile Term Code	Gap	Gap	Max	Hold	Max	
30th %ile Green (s)	26.2	26.2	6.0	37.2	12.0	
30th %ile Term Code	Gap	Gap	Max	Hold	Max	
10th %ile Green (s)	25.6	25.6	0.0	25.6	10.8	
10th %ile Term Code	Dwell	Dwell	Skip	Dwell	Gap	
Queue Length 50th (ft)	242	0		102	102	0
Queue Length 95th (ft)	384	27		137	#250	34
Internal Link Dist (ft)	520			420	720	
Turn Bay Length (ft)					100	
Base Capacity (vph)	1193	1090		1759	346	643
Starvation Cap Reductn	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0
Reduced v/c Ratio	0.64	0.20		0.66	0.76	0.20
Intersection Summary						

intersection Summar

Area Type: Other

Cycle Length: 73

Actuated Cycle Length: 63.3

Natural Cycle: 60

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.82 Intersection Signal Delay: 17.1

Intersection LOS: B

Lanes, Volumes, Timings 4: Salisbury Street & Main Street (Route 122A)

2024 No-Build Conditions Weekday Evening Peak Hour

Intersection Capacity Utilization 96.9%

Analysis Period (min) 15

90th %ile Actuated Cycle: 73

70th %ile Actuated Cycle: 72.7

50th %ile Actuated Cycle: 65.4

30th %ile Actuated Cycle: 59.2

10th %ile Actuated Cycle: 46.4

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Splits and Phases: 4: Salisbury Street & Main Street (Route 122A)

Third sitte i Hedes.	Todalobery Circle a Main Circle (Tobie 122A)	
Vro1	₹ 52	
HUGEN	45.5	
₩ ø6		* res
56s		17 s

ICU Level of Service F

Intersection	.8						
int Delay, s/veh 0	.0						
Movement	EBL	EBR	NE	L NBT	SBT	SBR	
Vol, veh/h	17	18		5 203	350	6	
Conflicting Peds, #/hr	0	0		0 0	0	0	
Sign Control	Stop	Stop	Fre	e Free	Free	Free	
RT Channelized	-	None		- None	'n	None	
Storage Length	0	14.			₩	-	
Veh in Median Storage, #	0	n n		- 0	0	-	
Grade, %	0	-		- 0	0	-	
Peak Hour Factor	92	92	9	92	92	92	
Heavy Vehicles, %	0	0		0 2	5	0	
Nvmt Flow	18	20		5 221	380	7	
Major/Minor	Minor2		Major	1	Major2		
Conflicting Flow All	616	384	38	7 0	-	0	W. C. C. C. C. C. C. C. C. C. C. C. C. C.
Stage 1	384	-			₩	-	
Stage 2	232	-				.	
Critical Hdwy	6.4	6.2	4.	1 -		-	
Critical Hdwy Stg 1	5.4	-			_	_	
Critical Hdwy Stg 2	5.4	-			_	-	
ollow-up Hdwy	3.5	3.3	2.	2 -	-	-	
ot Cap-1 Maneuver	457	668	118	3 -	_	-	
Stage 1	693	-				-	
Stage 2	811	-			-	-	
Platoon blocked, %				-	3 0	-	
Nov Cap-1 Maneuver	455	668	118	3 -		-	
Nov Cap-2 Maneuver	455	-			-	-	
Stage 1	693	-			-	-	
Stage 2	807	-			-	-	
pproach	EB	 	<u>N</u>		SB		
ICM Control Delay, s	12.1		0.	2	0		
ICM LOS	В						
/inor Lane/Major Mvmt	NBL	NBT EBLn1	SBT SB	R			
Capacity (veh/h)	1183	- 544	-	-			
ICM Lane V/C Ratio	0.005	- 0.07	-	_			
ICM Control Delay (s)	8.1	0 12.1	_	ou .			
ICM Lane LOS	A	A B	<u></u>				
ICM 95th %tile Q(veh)	0	- 0.2					

Intersection											
Int Delay, s/veh C	8.				************************			' '			
Movement	WBL	WBR		NB	Т :	NBR	SBL	SBT			
Vol, veh/h	4	4		5		1	1	31		· · · · · · · · · · · · · · · · · · ·	
Conflicting Peds, #/hr	0				0	0	0	0			
Sign Control	Stop	Stop		Fre	е	Free	Free	Free			
RT Channelized	`-	None None				lone		None			
Storage Length	0	-			-			-			
/eh in Median Storage, #	0	4		(0	_		0			
Grade, %	0				0	_	_	Ö			
Peak Hour Factor	92	92		9:		92	92	92			
łeavy Vehicles, %	2	2			2	2	2	2			
//vmt Flow	4	4		62		1	1	34			
//////////////////////////////////////	Minor1			Major′	1		Major2				
Conflicting Flow All	99	63		()	0	63	0			-
Stage 1	63	-			-	-	-	_			
Stage 2	36	-			-	-	-	_			
ritical Hdwy	6.42	6.22			-	-	4.12	_			
ritical Hdwy Stg 1	5.42	-				-	-				
ritical Hdwy Stg 2	5.42					-	_	-			
ollow-up Hdwy	3,518	3.318				_	2.218				
ot Cap-1 Maneuver	900	1002			-	_	1540	_			
Stage 1	960	-				_	, , , ,				
Stage 2	986	_				_	_	_			
latoon blocked, %				-		_					
lov Cap-1 Maneuver	899	1002				_	1540	_			
ov Cap-2 Maneuver	899			_		_	10.10				
Stage 1	960	_		_		_		_			
Stage 2	985	-		_			-	_			
								-			
oproach	WB			NB			SB		<u> </u>		
CM Control Delay, s	8.8			0			0.2				
CM LOS	Α										
inor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT							
apacity (veh/h)		- 948	1540	- OD I							
CM Lane V/C Ratio	_	- 0.009		-							
CM Control Delay (s)	_	- 8.8	7.3	0							
CM Lane LOS	_	- 0.6 - A	7.S A								
CM 95th %tile Q(veh)	-	- 0	0	Α							

··												
Int Delay, s/veh	12.3	, .								,		
Movement	EBL.	EBT	EBR	WBL	WBT	WBR	NB	_ NBT	NBR	SBL	SBT	SBF
Vol, veh/h	12	1206	15	17	582	15	1	2 0	49	3	0	4
Conflicting Peds, #/hr	0	0	0	0	0	0		0 0	0	0	0	(
Sign Control	Free	Free	Free	Free	Free	Free	Sto	s Stop	Stop	Stop	Stop	Stop
RT Channelized	-	_	None	-	-	None			None		-	None
Storage Length	-	-		-	-	-			-	-	-	
Veh in Median Storage,	# -	0	-	-	0	-		- 0	-		0	
Grade, %		-2	-	<u>.</u>	3	_		- 9	*	-	-6	
Peak Hour Factor	91	91	91	91	91	91	9	1 91	91	91	91	91
Heavy Vehicles, %	0	3	7	6	5	0		0 0	2	0	0	C
Mvmt Flow	13	1325	16	19	640	16	1	3 0	54	3	0	4
Major/Minor	Major1			Major2			Minor	1		Minor2		
Conflicting Flow All	656	0	0	1342	0	0	204		1334	2072	2053	648
Stage 1	-	-	-	1012	-	_	136		1001	685	685	0-10
Stage 2	_	_	_	_		_	68			1387	1368	_
Critical Hdwy	4.1	_		4.16		_	8.9		7.12	5.9	5.3	5.6
Critical Hdwy Stg 1	7.1	_		7.10	_	_	7.		1,,2	4.9	4.3	0.0
Critical Hdwy Stg 2	_	_	_	_	_	_	7.9		_	4.9	4.3	
Follow-up Hdwy	2.2	_	_	2.254	_	_	3.		3.318	3.5	4	3.3
Pot Cap-1 Maneuver	941	_	_	501	_	_	1:		135	80	111	528
Stage 1		_	_		-	_	9,		-	555	567	020
Stage 2	-	_	_	-	_	_	31:		_	284	342	
Platoon blocked, %		-			_	_	01.	- 011		20.	0,2	
Mov Cap-1 Maneuver	941		_	501	_	-	14	18	135	44	99	528
Mov Cap-2 Maneuver	-	_	_	-	_	-	14		.00	44	99	020
Stage 1	_	_		_	_	_	8		_	524	533	
Stage 2	-	-	-	•	-	-	29		-	161	323	_
Approach	EB			WB			NE	>		SB		
Approach				0.3								
HCM Control Delay, s HCM LOS	0.1			0.3			\$ 375.1 F			47.7 E		
Minor Lane/Major Mvmt	NBLn1	EBL.	EBT	EBR WBL	WBT	WBR S	BLn1					
Capacity (veh/h)	50	941		- 501	_	_	92				·, · · · · · · · · · · · · · · · · · ·	
ICM Lane V/C Ratio	1.341		_	- 0.037	-	_	0.084					
ICM Control Delay (s)	\$ 375.7	8.9	0	- 12.5	0		47.7					
HCM Lane LOS	F	Α.	Ā	- B	Ä		E					
HCM 95th %tile Q(veh)	6.2	0	-	- 0.1	-		0.3					
votes	0.2	v		V.1			V. V					
·: Volume exceeds capa	city \$: De	lay exc	eeds 30	00s +: Com	outation	Not De	fined *: A	l maior v	olume ir	ı platoon	· · · · · · · · · · · · · · · · · · ·	

		***	*	4	*	1
Lane Group	EBT	EBR	R WBL	WBT	NBL	NBR
Lane Configurations	<u>ተ</u>	**		413	NO.	
Voiume (vph)	983	266		499	111	109
Ideal Flow (vphp!)	1900	1900		1900	1900	1900
Lane Width (ft)	11	11			11	11
Grade (%)	-2%	,,	12	1%	-6%	11
Storage Length (ft)	-Z /0	0		170		•
Storage Lanes					100	0
Taper Length (ft)		1	_		1	1
	4.00	4.00	25	0.00	25	
Lane Util. Factor	1.00	1.00		0.95	1.00	1.00
Frt		0.850				0.850
Flt Protected				0.992	0.950	
Satd. Flow (prot)	1801	1531	0	3344	1797	1531
Fit Permitted				0.546	0.950	
Satd. Flow (perm)	1801	1531	0	1841	1797	1531
Right Turn on Red		Yes				Yes
Satd. Flow (RTOR)		296				116
Link Speed (mph)	30			30	30	
Link Distance (ft)	600			500	800	
Travel Time (s)	13,6			11.4	18.2	
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90
Heavy Vehicles (%)	3%	3%	4%	7%	0%	5%
Adj. Flow (vph)	1092	296	100	554	123	121
Shared Lane Traffic (%)	1002	230	100	554	123	121
Lane Group Flow (vph)	1092	296	0	GE A	100	404
Enter Blocked Intersection	No			654 N=	123	121
Lane Alignment		No	No	No	No	No
	Left	Right	Left	Left	Left	Right
Median Width(ft)	0			0	11	
Link Offset(ft)	0			0	0	
Crosswalk Width(ft)	16			16	16	
Two way Left Turn Lane						
Headway Factor	1.03	1.03	1.01	1.01	1.01	1.01
Turning Speed (mph)		9	15		15	9
Number of Detectors	1	1	1	1	1	1
Detector Template						
Leading Detector (ft)	50	50	50	50	50	50
Trailing Detector (ft)	0	0	0	0	0	0
Detector 1 Position(ft)	Ö	ŏ	Ö	0	0	0
Detector 1 Size(ft)	50	50	50	50	50	50
Detector 1 Type	Cl+Ex	Cl+Ex	CI+Ex	CI+Ex	CI+Ex	CI+Ex
Detector 1 Channel	OITEX	OI LEX	OI LX	OLLY	OI LEX	∪ I⊤EX
Detector 1 Extend (s)	0.0	0.0	0.0	0.0	0.0	0.0
Detector 1 Queue (s)		0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	0.0	0.0
Detector 1 Delay (s)	0.0	0.0	0.0	0.0	0.0	0.0
Turn Type	NA	Perm	pm+pt	NA	Prot	pt+ov
Protected Phases	2		1	6	8	81
Permitted Phases		2	6			
Detector Phase	2	2	1	6	8	8 1
Switch Phase						
Minimum Initial (s)	10.0	10.0	6.0	10.0	6.0	

G:\Projects\1038 - Holden (Pine Tree)\Synchro\1038 B AM.syn MDM Transportation Consultants, Inc

	 - -	*	*	**	*	<i>*</i>
Lane Group	EBT	EBR	WBL	WBT	NBL	NBR
Minimum Split (s)	15.0	15.0	11.0	15.0	11.0	
Total Split (s)	70.0	70.0	11.0	81.0	20.0	
Total Split (%)	69.3%	69.3%	10.9%	80,2%	19.8%	
Maximum Green (s)	65.0	65.0	6.0	76.0	15.0	
Yellow Time (s)	4.0	4.0	4.0	4.0	4.0	
All-Red Time (s)	1.0	1.0	1.0	1.0	1.0	
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	
Total Lost Time (s)	5.0	5.0		5.0	5.0	
Lead/Lag	Lag	Lag	Lead			
Lead-Lag Optimize?	3	3				
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	
Recall Mode	Min	Min	None	Min	None	
Act Effct Green (s)	60.6	60.6	110,10	71.7	11.5	22.6
Actuated g/C Ratio	0.65	0.65		0.77	0.12	0.24
v/c Ratio	0.93	0.27		0.43	0.56	0.26
Control Delay	30.9	1.5		4.2	49.9	8,1
Queue Delay	0.0	0.0		0.0	0.0	0.0
Total Delay	30.9	1.5		4.2	49.9	8.1
LOS	C	A		A	D	A
Approach Delay	24.6	,,		4.2	29.1	• •
Approach LOS	C			Α	C	
90th %ile Green (s)	65.0	65.0	6.0	76,0	15.0	
90th %ile Term Code	Max	Max	Max	Hold	Max	
70th %ile Green (s)	65.0	65.0	6.0	76.0	14.0	
70th %ile Term Code	Max	Max	Max	Hold	Gap	
50th %ile Green (s)	65.0	65.0	6.0	76.0	12.0	
50th %ile Term Code	Max	Max	Max	Hold	Gap	
30th %ile Green (s)	59.9	59.9	6.0	70.9	10.0	
30th %ile Term Code	Gap	Gap	Max	Hold	Gap	
10th %ile Green (s)	48.6	48.6	6.0	59.6	7.2	
10th %ile Term Code	Dwell	Dwell	Max	Dwell	Gap	
Queue Length 50th (ft)	521	0	IIIMA	47	73	2
Queue Length 95th (ft)	#937	28		74	131	46
Internal Link Dist (ft)	520	20		420	720	-10
Turn Bay Length (ft)	020			720	100	
Base Capacity (vph)	1267	1165		1612	291	441
Starvation Cap Reductn	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0
Reduced v/c Ratio	0.86	0.25		0.41	0.42	0.27
	0.00	0,20		U.T I	V.7£	0.41
Intersection Summary						

Area Type: Other

Cycle Length: 101

Actuated Cycle Length: 93,3

Natural Cycle: 80

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio: 0.93 Intersection Signal Delay: 19.3

Intersection LOS: B

Intersection Capacity Utilization 86.8%

ICU Level of Service E

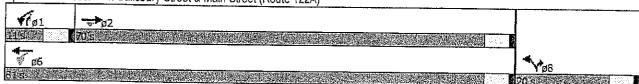
Analysis Period (min) 15

90th %ile Actuated Cycle: 101 70th %ile Actuated Cycle: 100 50th %ile Actuated Cycle: 98

30th %ile Actuated Cycle: 90.9 10th %ile Actuated Cycle: 76.8

95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

Splits and Phases: 4: Salisbury Street & Main Street (Route 122A)



Intersection						············		
	0.6							
Movement	EBL	EBR	NBL	NBT	SBT	SBR		
Vol, veh/h	11	10	19	379	356	18		
Conflicting Peds, #/hr	0	0	0	0	0	0		
Sign Control	Stop	Stop	Free	Free	Free	Free		
RT Channelized	-	None	-	None	-	None		
Storage Length	0	-	-	-	-	-		
Veh in Median Storage, #	0	-	-	0	0	-		
Grade, %	0	-	-	0	0	-		
Peak Hour Factor	92	92	92	92	92	92		
Heavy Vehicles, %	0	0	0	2	5	0		
Mvmt Flow	12	11	21	412	387	20		
Major/Minor	Minor2		Major1		Major2			
Conflicting Flow All	850	397	407	0	-	0		
Stage 1	397	-	-	-	_	-		
Stage 2	453	-	_	-	-	-		
Critical Hdwy	6.4	6.2	4.1	-	m.	-		
Critical Hdwy Stg 1	5.4			_		_		
Critical Hdwy Stg 2	5.4	-	_	_	_	-		
Follow-up Hdwy	3.5	3.3	2.2	***	-			
Pot Cap-1 Maneuver	334	657	1163	-		_		
Stage 1	683	_	-	-		-		
Stage 2	645	_	-	•	_			
Platoon blocked, %				-		_		
Mov Cap-1 Maneuver	326	657	1163	-	_	*1		
Mov Cap-2 Maneuver	326	-	-	_	_	-		
Stage 1	683	-	-	-	_	_		
Stage 2	630	-	-	-	-	-		
Approach	EB		NB		SB			
HCM Control Delay, s	13.9		0.4		0		·	·····
HCM LOS	15.5 B		0.4		U			
Minor Lane/Major Mvmt	NBL	NBT EBLn1	SBT SBR					
Capacity (veh/h)	1163	- 429	OD: ODIY		· · · · · · · · · · · · · · · · · · ·			
HCM Lane V/C Ratio	0.018	- 0.053						
HCM Control Delay (s)	8.2	0.053						
-iCM Lane LOS	6.2 A		* -					
HCM 95th %tile Q(veh)	0.1	A B - 0.2						
IOINI SOUL VIIIIE (KIVEIL)	V, I	- U.Z						

Intersection	_	-								
Int Delay, s/veh	0.5									
Movement	WBL	. WBR		NBT	NBR	SBL	SBT			
Vol, veh/h	2			40	4	4	62			
Conflicting Peds, #/hr	0			Ő	0	0	0			
Sign Control	Stop	•		Free	Free	Free	Free			
RT Channelized				1100	None	1100	None			
Storage Length	0	-		-	140110	_	HOHE			
Veh in Median Storage, #		_		0	_	_	0			
Grade, %	Ō	_		0	- -	-	0			
Peak Hour Factor	92	92		92	92	92	92			
Heavy Vehicles, %	2	2		2	2	2	2			
Mvmt Flow	2	2		43	4	4	67			
	_	L		70	7	4	07			
Major/Minor	Minor1			Major1		Majoro				
Conflicting Flow All	122	46	·····	- Major 1	0	Major2				
Stage 1	46	40		U		48	0			
Stage 2	76	_		-	-	-	-			
Critical Hdwy	6.42	6.22		-	-	4.40	•			
Critical Hdwy Stg 1	5.42	0,22			_	4.12	-			
Critical Hdwy Stg 2	5.42	-		-	-	-	-			
Follow-up Hdwy	3.518	3.318		-	*	0.040	-			
Pot Cap-1 Maneuver	873	1023		=	-	2.218	-			
Stage 1	976	1023			-	1559	-			
Stage 2	947	-		-	-	-	-			
Platoon blocked, %	<i>341</i>	-		-	-	-	-			
Mov Cap-1 Maneuver	870	1023		-	-		-			
Mov Cap-1 Maneuver	870 870				-	1559	-			
Stage 1	976	-		-	-	-	-			
Stage 2	944	-		F	-	-				
Olage Z	944	7		-	-	•	-			
Approach	WB			NΒ		SB				
HCM Control Delay, s	8.8		······································	0			·			
HCM LOS	Α			V		0.4				
	, (
Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL S	ВТ						
Capacity (veh/h)	_		1559			·+···		·····		
HCM Lane V/C Ratio	-	- 0.005 (_						
HCM Control Delay (s)	-	- 8.8	7.3	0						
HCM Lane LOS	_	- 0.6 - A								
HCM 95th %tile Q(veh)	- 	- 0	A 0	A						
TOTAL OUT THE OUT OF VOIT	-	- U	V	•						

Intersection												
Int Delay, s/veh 1	2.2											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NE	BL NBT	NBR	SBL	SBT	SBF
Vol, veh/h	12	851	32	34	1223	15		9 1	32	12	0	23
Conflicting Peds, #/hr	0	0	0	0	0	0		0 0	0	0	0	0
Sign Control	Free	Free	Free	Free	Free	Free	Ste	p Stop	Stop	Stop	Stop	Stop
RT Channelized	-	-	None	-	-	None			None	-	-	None
Storage Length	-	_	-	-	-	-			-	-	-	
Veh in Median Storage, #	-	0	-	-	0	-		- 0		-	0	•
Grade, %	. •	-2	-	-	3	**		- 9		-	-6	
Peak Hour Factor	97	97	97	97	97	97	!	7 97	97	97	97	97
Heavy Vehicles, %	0	1	0	3	1	7		0 0		8	0	0
Mvmt Flow	12	877	33	35	1261	15		9 1	33	12	0	24
Major/Minor	Major1			Major2			Mino	r1		Minor2		
Conflicting Flow All	1276	0	0	910	0	0	22		894	2275	2274	1269
Stage 1	12,0	-	-	-	-	-	9			1339	1339	-
Stage 2	_	_	_	-	_	_	13			936	935	_
Critical Hdwy	4.1		_	4.13		-		.9 8.3		5.98	5.3	5.6
Critical Hdwy Stg 1		_	_		_			.9 7.3		4.98	4.3	-
Critical Hdwy Stg 2		_	_	-	_	-		9 7.3	_	4.98	4.3	_
Follow-up Hdwy	2.2	_		2.227	μ.	_		,5 4	3.363	3.572	4	3.3
Pot Cap-1 Maneuver	551	_		744	_	_		9 13		58	87	256
Stage 1	-	_	_	, , ,	_	_	20			286	349	
Stage 2	_	_	_	_		_		95 113		424	474	_
Platoon blocked, %		_	_		_		,	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		,	,,,	
Mov Cap-1 Maneuver	551	_	_	744		_	_	7 10	266	40	70	256
Mov Cap-2 Maneuver	-			7 -7-1		_		7 10		40	70	
Stage 1	-			_		_		8 213		273	292	_
Stage 2		-	-		-	-		2 95		353	453	
Annranch	EB			WB			· N	ΙΒ		SB		
Approach	0.2						\$ 579		· · · · · · · · · · · · · · · · · · ·	69.5		
HCM Control Delay, s HCM LOS	U.Z			0.3			ង្ ១/ ៩	F		09.5 F		
					1425-	u Inn	001 4					
Minor Lane/Major Mvmt	NBLn1	EBL	EBT	EBR WBL	WBT	WBR:			 			· · · · · · · · · · · · · · · · · · ·
Capacity (veh/h)	28	551	-	- 744	-	-	90					
HCM Lane V/C Ratio		0.022	-	- 0.047	-		0.401					
HCM Control Delay (s)	\$ 579.9	11.7	0	- 10.1	0	_	69.5					
HCM Lane LOS	F	В	Α	- B	Α	-	F					
HCM 95th %tile Q(veh)	5.1	0.1	-	- 0.1	-	-	1.6					
Notes												
~: Volume exceeds capac	ity \$: De	elay exc	eeds 30	00s +: Com	putation	n Not De	efined *;	All major	volume i	n platoon		. –

					***************************************	,	-
	,	~	سمعد	******	*	<i>*</i>	×
		*	₹		,	1	
Lane Group	EBT	EBR	WBL	WBT	NBL	NBR	ζ
Lane Configurations	†	7		414	ja,	ሻ	
Volume (vph)	736	213		987	258	132	
ideal Flow (vphpl)	1900	1900		1900	1900	1900	
Lane Width (ft)	11	11		12	11	11	
Grade (%)	-2%		12	1%		1.1	
Storage Length (ft)	-2 /0	^	۸	1 70	-6%		
		0			100	0	
Storage Lanes		1	-		1	1	
Taper Length (ft)			25		25		
Lane Util. Factor	1.00	1.00		0.95	1.00	1.00	
Frt		0.850				0.850	ł
Flt Protected				0.993	0.950		
Satd. Flow (prot)	1837	1561	0	3531	1779	1592	,
Flt Permitted		,	•	0.557	0.950	.OUL	
Satd. Flow (perm)	1837	1561	0	1981	1779	1592	,
Right Turn on Red	1007		U	1301	1119		
=		Yes				Yes	
Satd. Flow (RTOR)		220				136	
Link Speed (mph)	30			30	30		
Link Distance (ft)	600			500	800		
Travel Time (s)	13.6			11.4	18,2		
Peak Hour Factor	0.97	0.97	0.97	0.97	0.97	0.97	
Heavy Vehicles (%)	1%	1%	1%	1%	1%	1%	
Adj. Flow (vph)	759	220	166	1018	266	136	
Shared Lane Traffic (%)	100		100	1010	200	100	
Lane Group Flow (vph)	759	ววก	٥	1101	200	400	
Enter Blocked Intersection		220	0	1184	266	136	
	No	No	No	No	No	No	
Lane Alignment	Left	Right	Left	Left	Left	Right	
Median Width(ft)	0			0	11		
Link Offset(ft)	0			0	0		
Crosswalk Width(ft)	16			16	16		
Two way Left Turn Lane				. •	. •		
Headway Factor	1.03	1.03	1.01	1.01	: 1.01	1.01	
Turning Speed (mph)	1100			1.01			
Number of Detectors		9	15	4	15	9	
	1	1	1	1	1	1	
Detector Template							
Leading Detector (ft)	50	50	50	50	50	50	
Trailing Detector (ft)	0	0	0	0	0	0	
Detector 1 Position(ft)	0	0	0	0	0	0	
Detector 1 Size(ft)	50	50	50	50	50	50	
Detector 1 Type	Cl+Ex	CI+Ex	Cí+Ex	CI+Ex	CI+Ex	Cl+Ex	
Detector 1 Channel	OI - LX	OI · ∟∧	OLILA	OI LEX	OFFEX	OUTEX	
Detector 1 Extend (s)	Λ.0	0.0	^ ^				
	0.0	0.0	0.0	0.0	0.0	0.0	
Detector 1 Queue (s)	0.0	0.0	0.0	0.0	0.0	0.0	
Detector 1 Delay (s)	0.0	0.0	0.0	0.0	0.0	0.0	
Turn Type	NA	Perm	pm+pt	NA	Prot	pt+ov	
Protected Phases	2		1	6	8	81	
Permitted Phases		2	6	-	•	J ,	
Detector Phase	2	2	1	6	8	8 1	
Switch Phase	۷.	4	1	U	o	ΟI	
Minimum Initial (s)	10.0	40.0	0.0	40.0	6.0		
សាមហាសាអ អេវាជា (2)	10.0	10.0	6.0	10.0	6.0		

G:\Projects\1038 - Holden (Pine Tree)\Synchro\1038 B PM.syn MDM Transportation Consultants, Inc.

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Lane Group	EBT	EBR	WBL	WBT	NBL	NBR
Minimum Split (s)	15.0	15.0	11.0	15.0	11.0	
Total Split (s)	45.0	45.0	11.0	56.0	17.0	
Total Split (%)	61.6%	61.6%	15.1%	76.7%	23.3%	
Maximum Green (s)	40.0	40.0	6.0	51.0	12.0	
Yellow Time (s)	4,0	4.0	4.0	4.0	4.0	
All-Red Time (s)	1.0	1.0	1.0	1.0	1.0	
Lost Time Adjust (s)	0.0	0.0		0.0	0.0	
Total Lost Time (s)	5.0	5.0		5.0	5.0	
Lead/Lag	Lag	Lag	Lead			
Lead-Lag Optimize?						
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	
Recall Mode	Min	Min	None	Min	None	
Act Effct Green (s)	33.0	33,0		41.4	12.1	23.4
Actuated g/C Ratio	0.52	0.52		0.65	0.19	0.37
v/c Ratio	0.80	0.24		0.85	0.79	0.20
Control Delay	20.7	2.1		13.7	47.6	4.8
Queue Delay	0.0	0.0		0.0	0.0	0.0
Total Delay	20.7	2.1		13.7	47.6	4.8
LOS	С	Α		В	D	Α
Approach Delay	16.5			13,7	33.2	
Approach LOS	В			В	С	
90th %ile Green (s)	40.0	40.0	6.0	51.0	12.0	
90th %ile Term Code	Max	Max	Max	Max	Max	
70th %ile Green (s)	40.0	40.0	6.0	51.0	12.0	
70th %ile Term Code	Hold	Hold	Max	Max	Max	
50th %ile Green (s)	32.7	32.7	6.0	43.7	12.0	
50th %ile Term Code	Hold	Hold	Max	Gap	Max	
30th %ile Green (s)	26.2	26,2	6.0	37.2	12.0	
30th %ile Term Code	Gap	Gap	Max	Hold	Max	
10th %ile Green (s)	26.4	26.4	0.0	26.4	11,1	
10th %ile Term Code	Dwell	Dwell	Skip	Dwell	Gap	
Queue Length 50th (ft)	243	0	٠٢	104	104	0
Queue Length 95th (ft)	385	27		139	#252	35
Internal Link Dist (ft)	520	2.1		420	720	00
Turn Bay Length (ft)	020			120	100	
Base Capacity (vph)	1183	1084		1709	343	644
Starvation Cap Reductn	0	0		0	0	0
Spillback Cap Reductn	0	0		0	0	0
Storage Cap Reductn	0	0		0	0	0
Reduced v/c Ratio	0.64	0.20		0.69	0.78	0.21
Loanood Mo Lano	0.04	0.20		0,00	0.70	U.Z.I
Intersection Summary						

Intersection Summary

Area Type: Other

Cycle Length: 73

Actuated Cycle Length: 63.7

Natural Cycle: 60

Control Type: Actuated-Uncoordinated

Maximum v/c Ratio; 0.85 Intersection Signal Delay; 17.8

Intersection LOS: B

Lanes, Volumes, Timings 4: Salisbury Street & Main Street (Route 122A)

2024 Build Conditions Weekday Evening Peak Hour

Intersection Capacity Utilization 97.5%

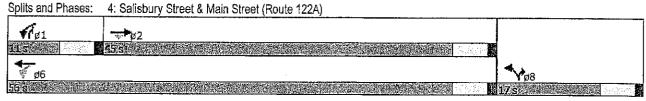
ICU Level of Service F

Analysis Period (min) 15
90th %ile Actuated Cycle: 73
70th %ile Actuated Cycle: 73
50th %ile Actuated Cycle: 65.7
30th %ile Actuated Cycle: 59.2
10th %ile Actuated Cycle: 47.5

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

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